

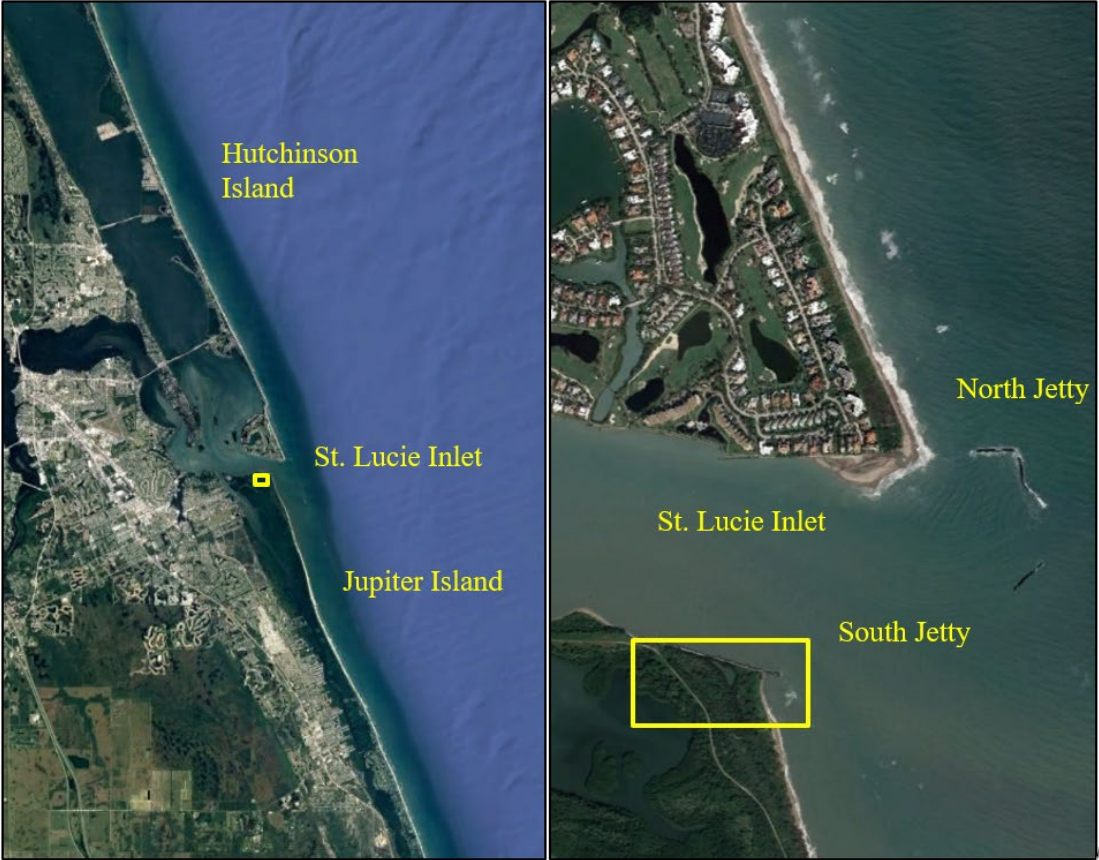
# DRONE TECHNOLOGY AND RUBBLE MOUND STRUCTURES

## ST. LUCIE INLET SOUTH JETTY CASE STUDY

Presented By: Andrew Wycklendt, P.E.



# PROJECT LOCATION



# PROBLEM IDENTIFICATION



## › June 2019 Engineering Investigation

- Level 1 Evaluation – 100% Structure
- Level 2 Evaluation – 10% Structure (i.e. profiles every 100 feet)
- Condition Rating = Fair; primary structure elements are sound, but minor to moderate defects or deterioration was observed

## › March 2020 Post-Dorian Drone Assessment

- Negligible change to breach, crest elevation, and side slopes

# AVAILABLE DATA

## › Geophysical

- Various LiDAR Surveys (USACE, FEMA, NASA, NOAA, NGS, USGS)
- April 2019 Jetty Assessment Surveys (RTK, Drone, and Laser Scan)
- October 2019 Post-Storm (i.e. Hurricane Dorian) Drone Survey

## › Oceanographic

- NOAA Water Level Observation Network
- FEMA Flood Insurance Study
- USACE Wave Information Studies

## › Engineering

- Design Drawings (1978)
- As-Built Drawings (1984)



# DESIGN CONDITIONS

- › Navigation Channel
  - Authorized Depth = -10 ft MLW
  - Required Overdepth = -12 ft MLW
- › Depth Limited Breaking
  - Breaking Height = 11.5 ft @ MHW
  - Equivalent to Annual Wave Height
- › Design Template
  - No Curve
  - Baseline = Maintenance Road
  - Crest = 10 ft @ 5.65 ft NAVD (8.0 ft MLW)
  - 5 Platforms (Width = 25', Protrusion = 15')
  - Slope = 1V:2H
- › Armor Stone Size
  - Hudson (1974) Stability Equation
    - Irregular head-on waves
  - Stability Coefficient = 2.0
    - Rough angular stone shape
    - Random Placement
    - Breaking waves
  - Waves Breaking on Crest
    - Crest Elevation = 5.65 ft NAVD
  - Armor Stone Size
    - 5.6 to 9.3 tons (7.4 tons)
    - 4.1 to 4.8 feet (4.5 feet)
  - Core Stone Size
    - 0.56 to 0.93 tons (0.74 tons)
    - 1.9 to 2.2 feet (2.1 feet)



Orthorectified Photomosaic



Orthorectified Photomosaic



Orthorectified Photomosaic





Orthorectified Photomosaic



Orthorectified Photomosaic



Orthorectified Photomosaic



Orthorectified Photomosaic



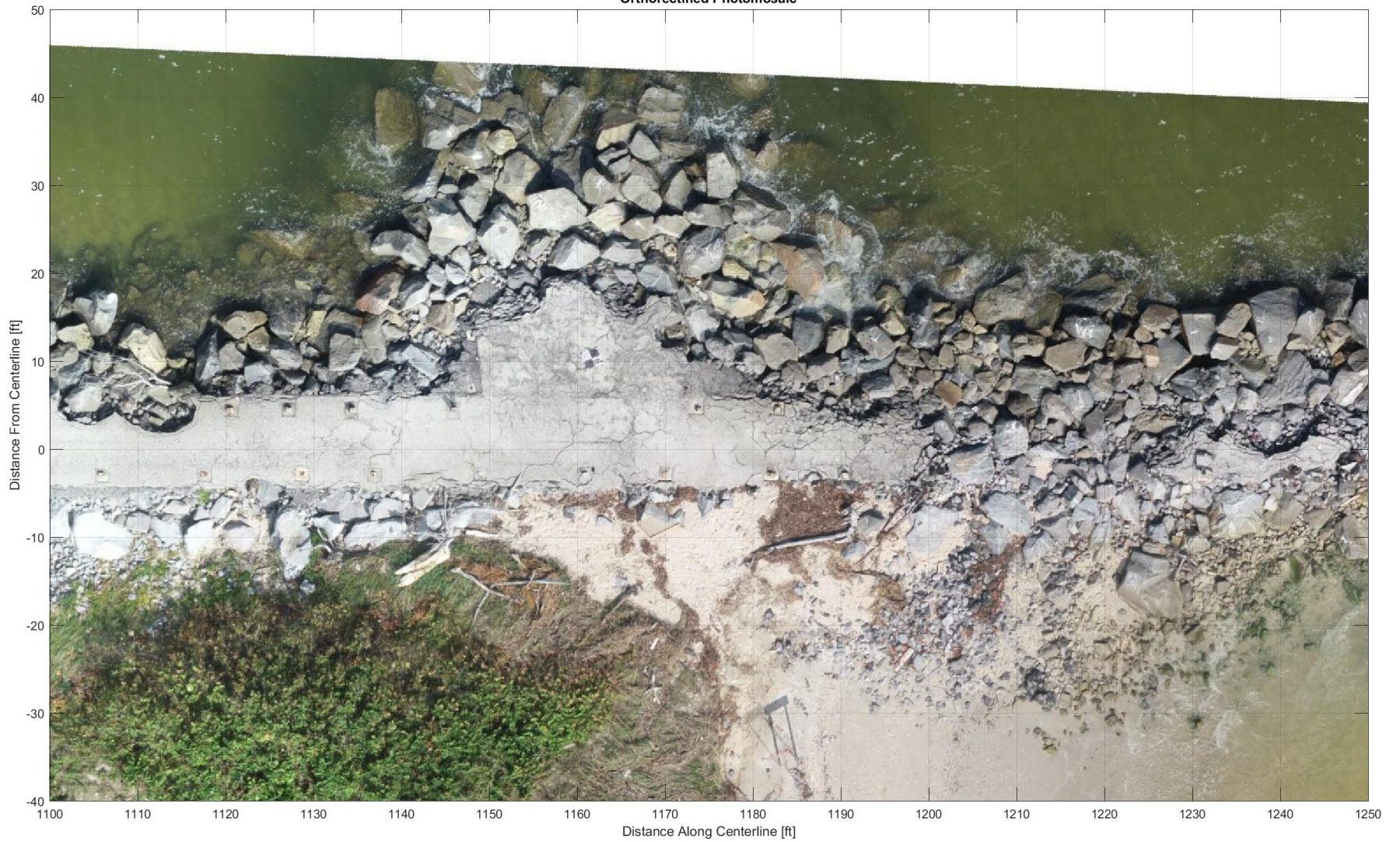
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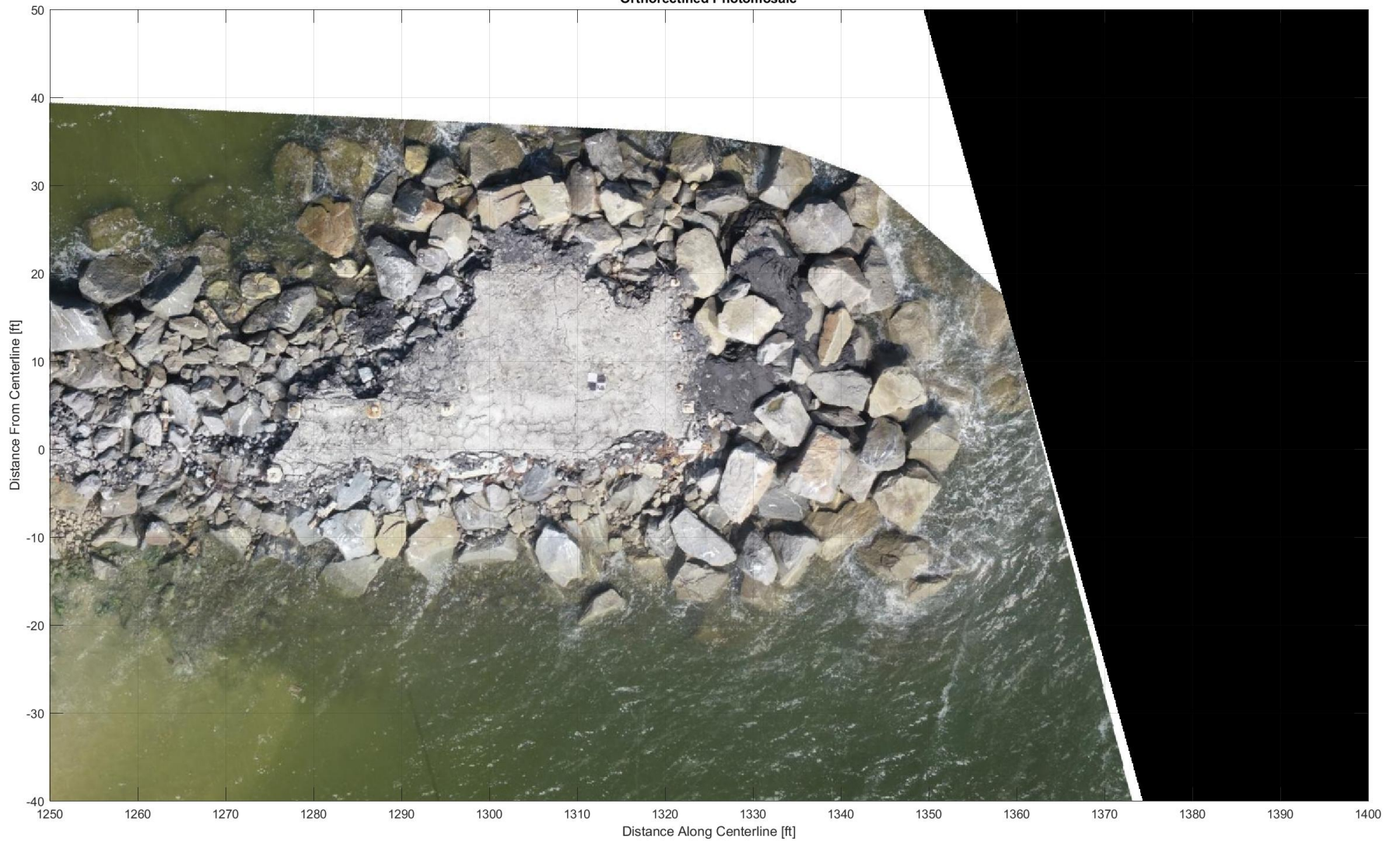
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Orthorectified Photomosaic

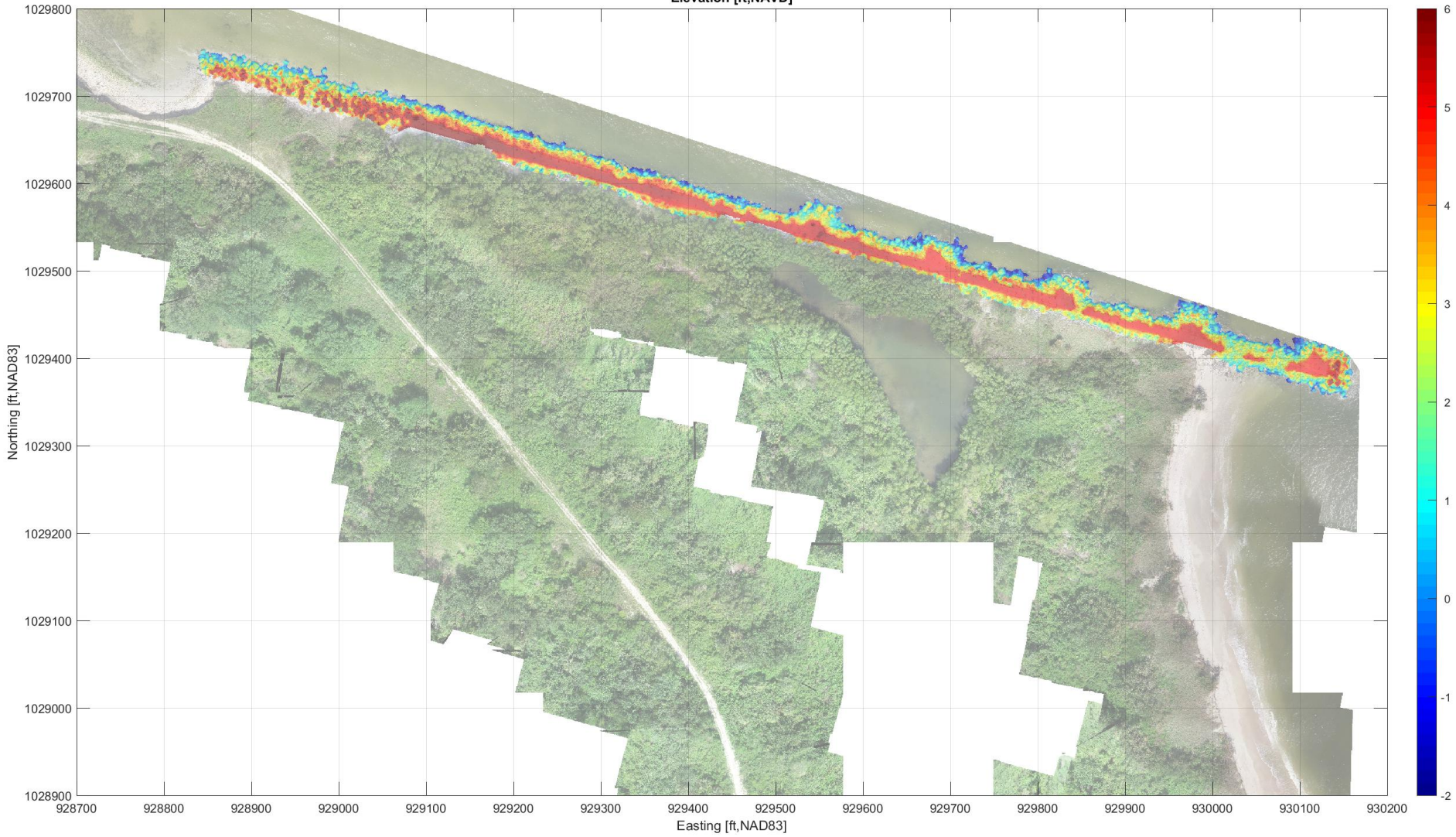


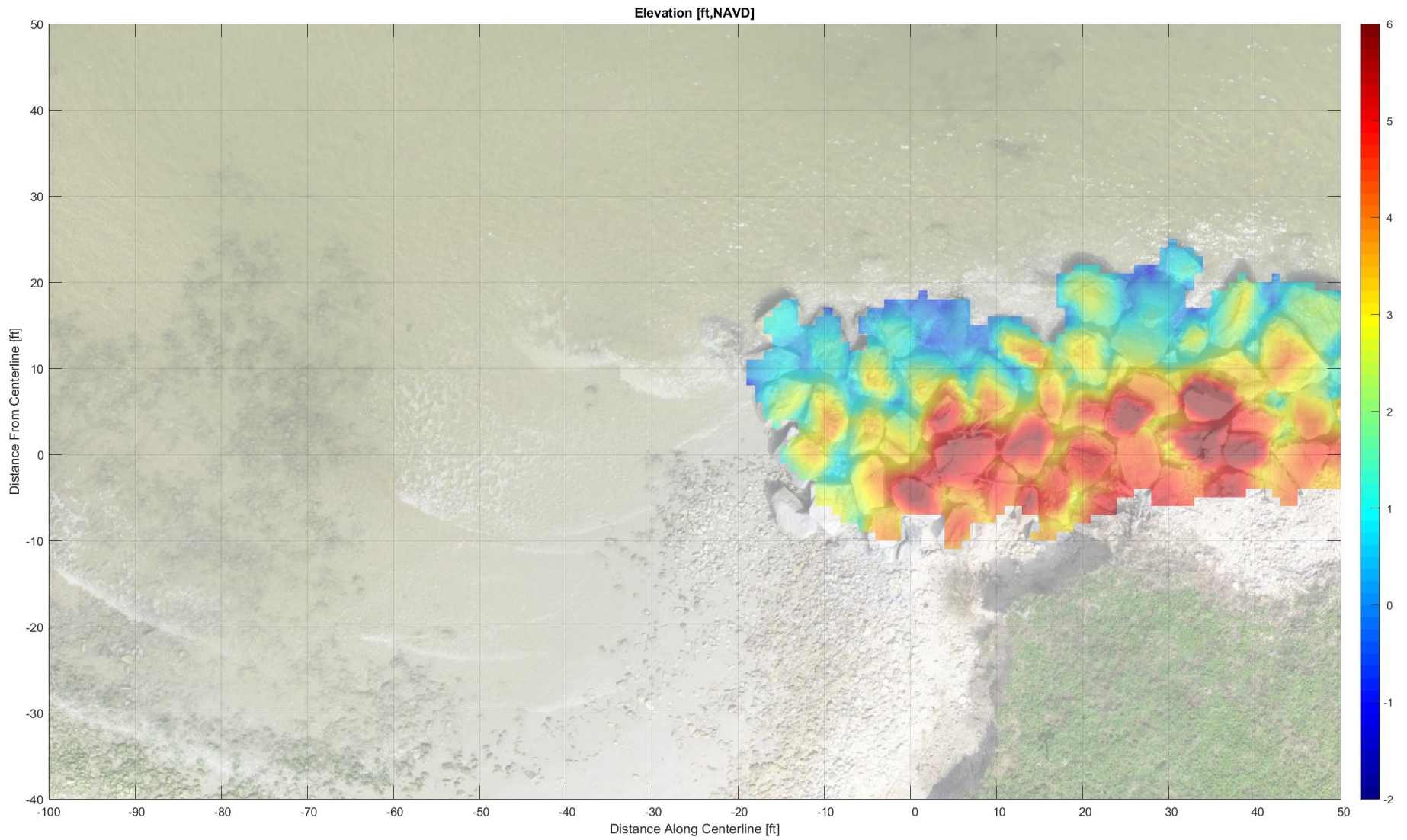
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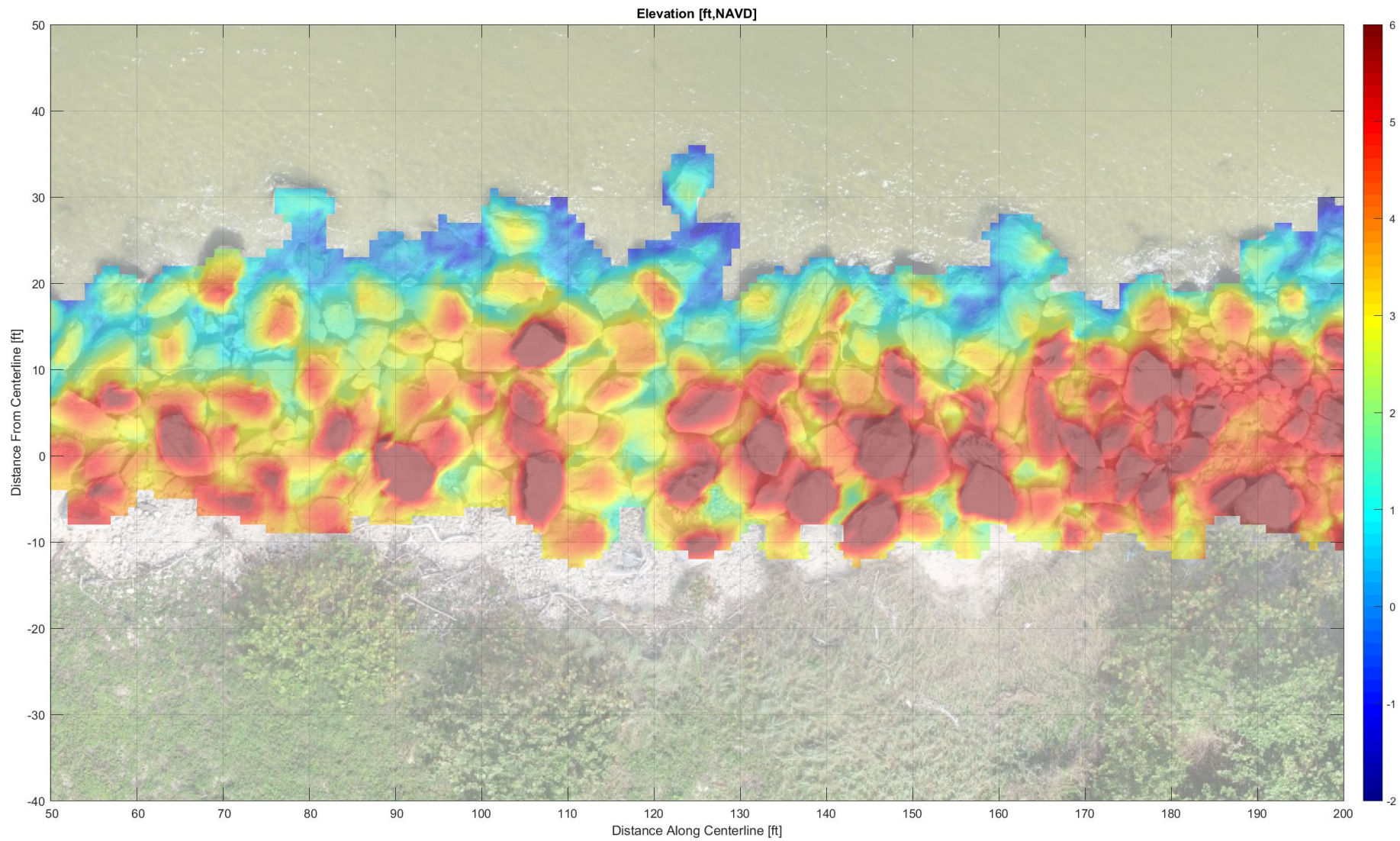


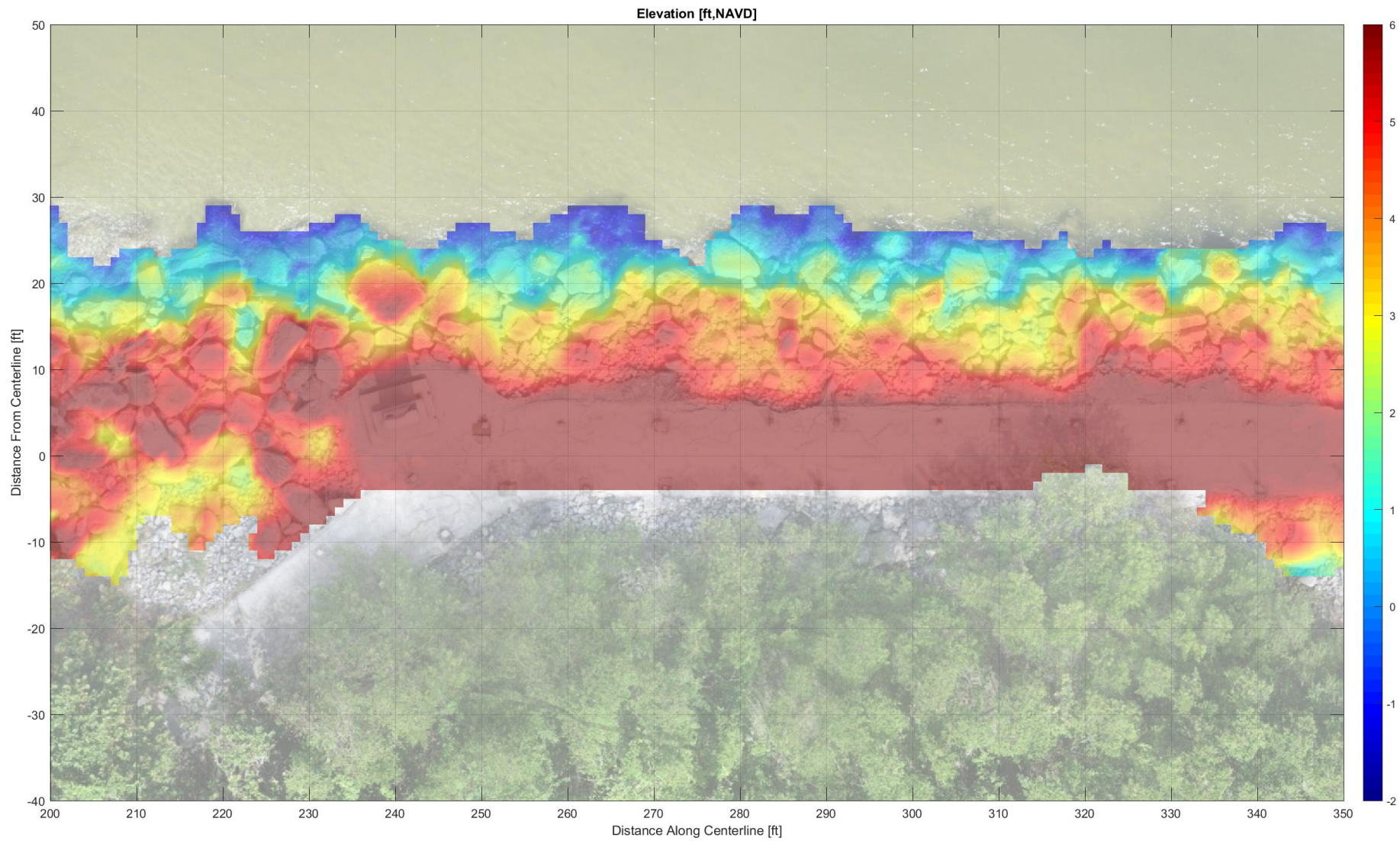


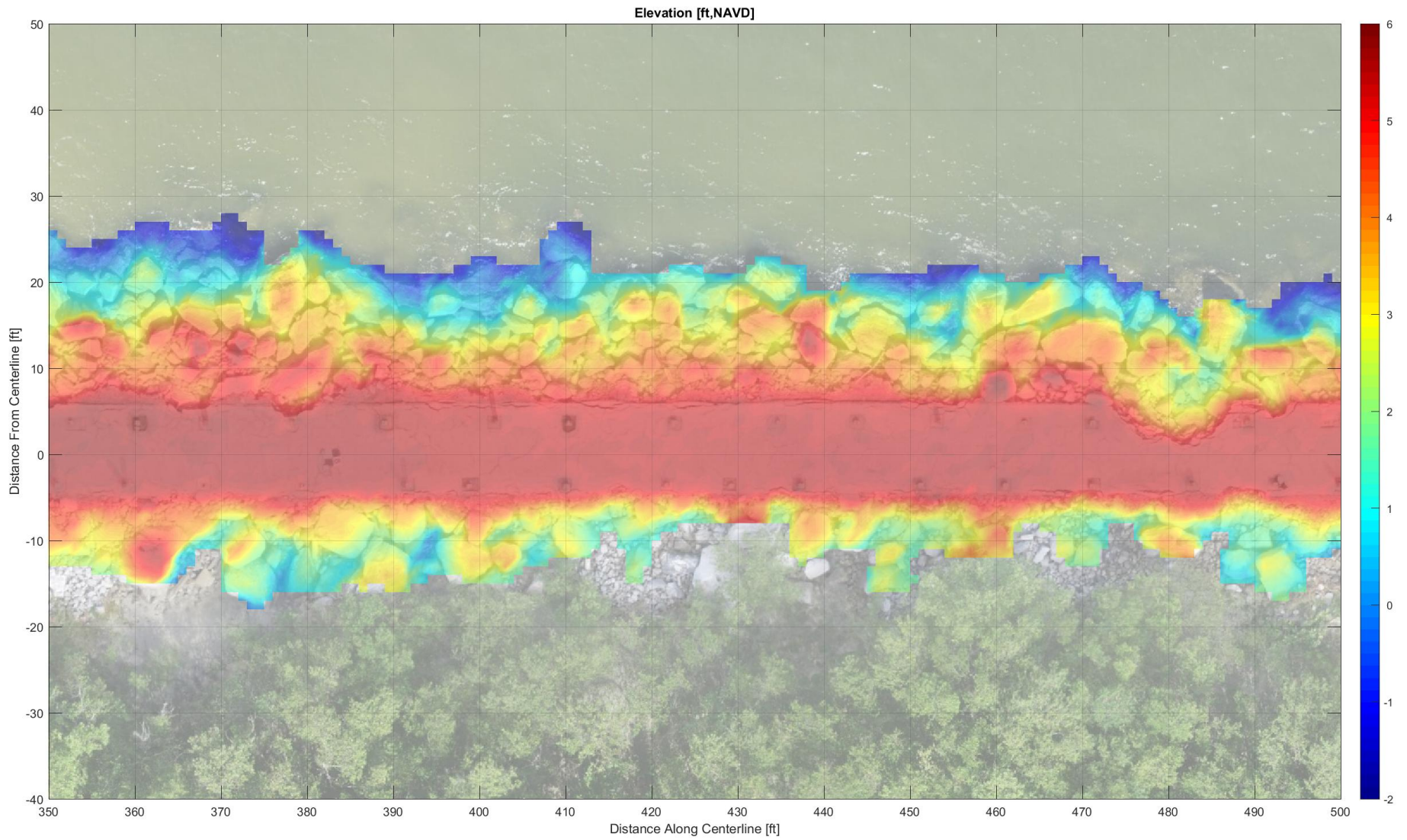
Elevation [ft,NAVD]

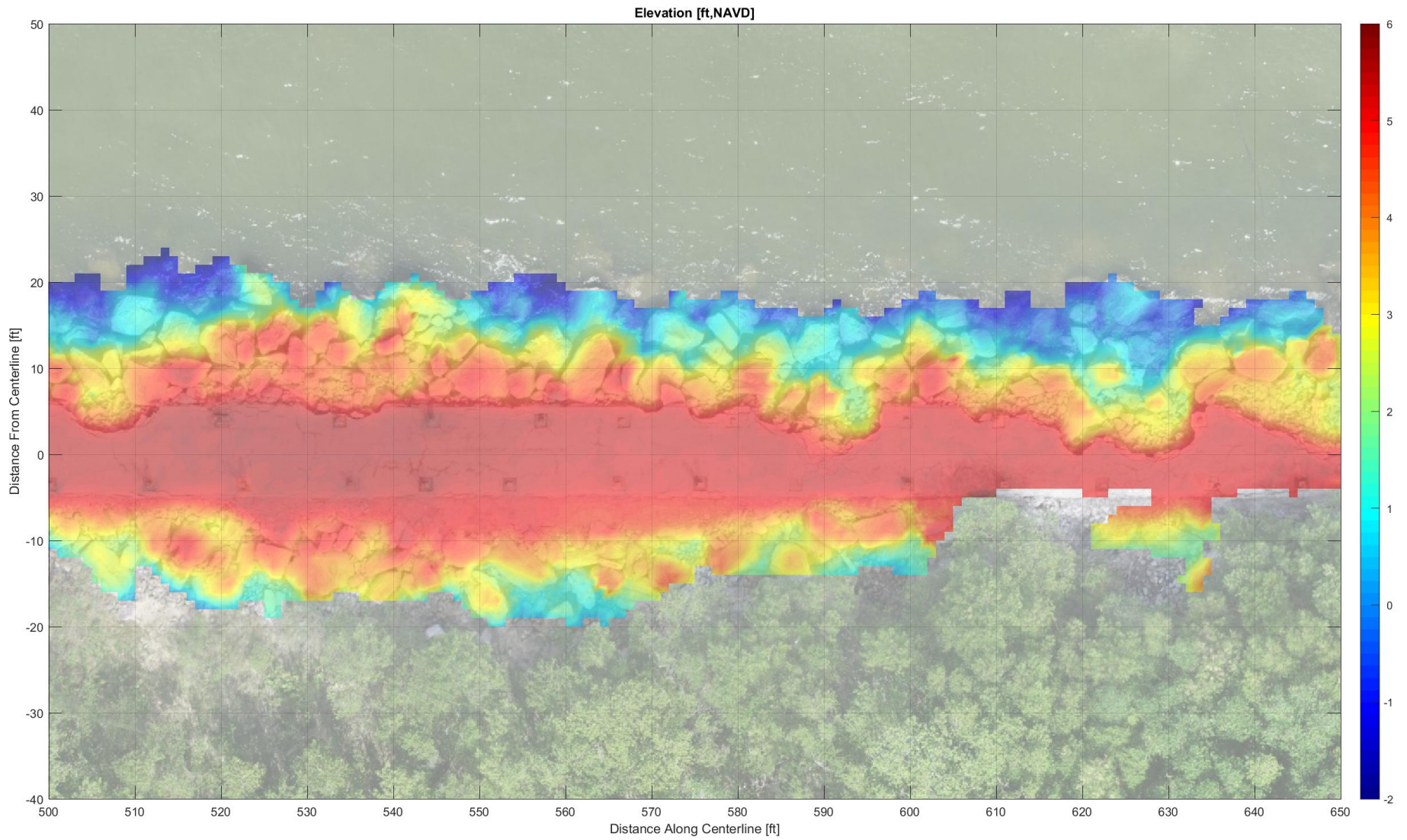


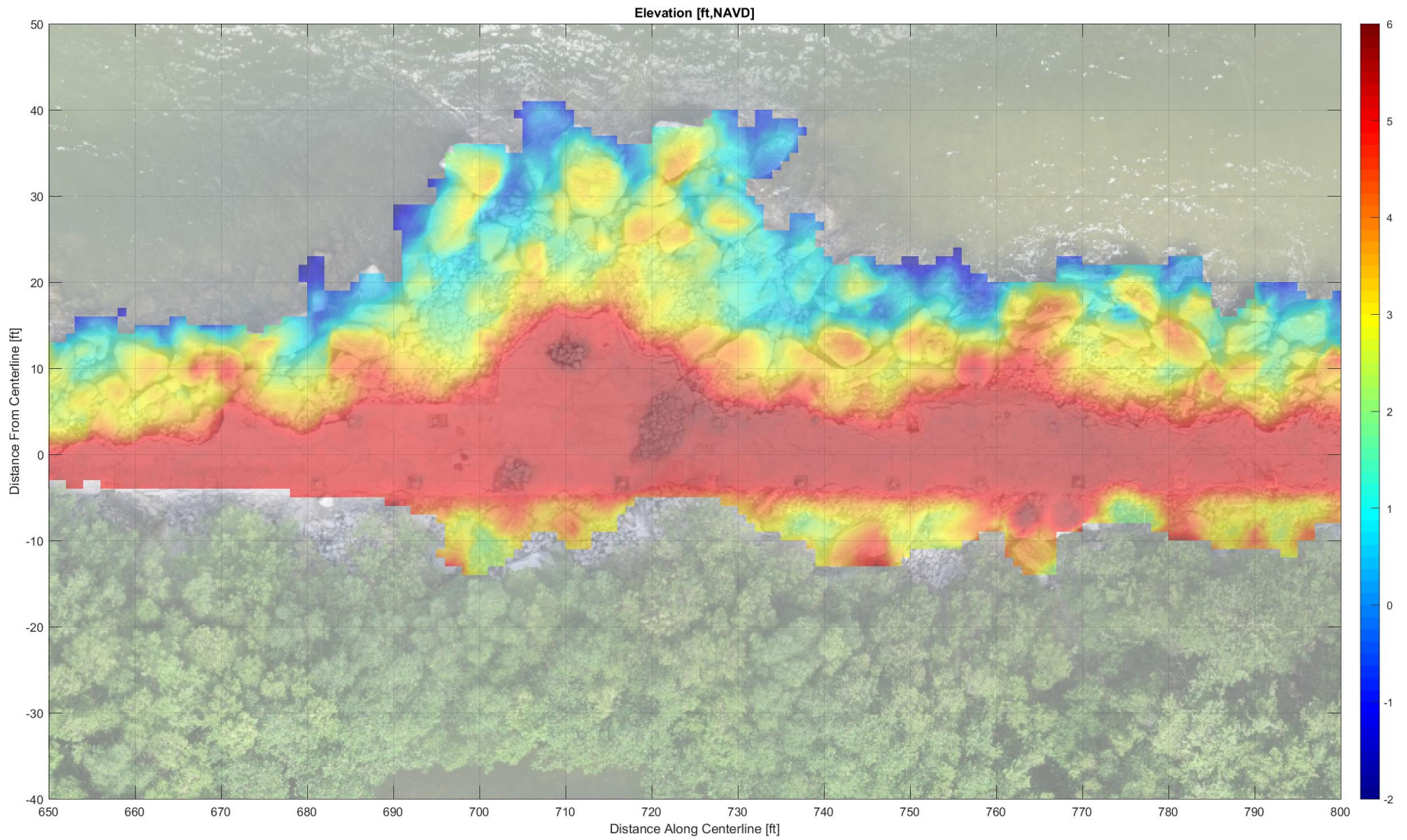


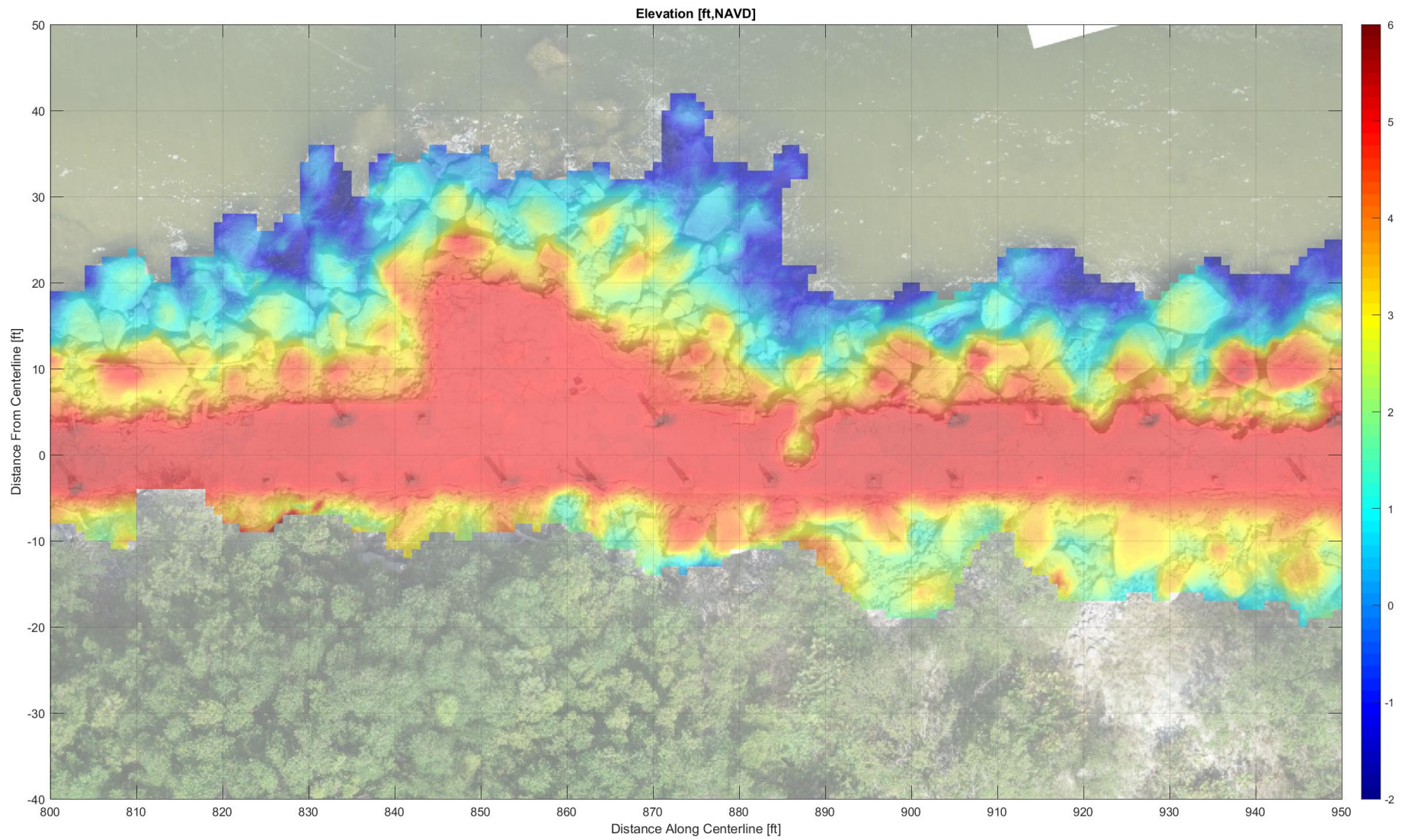




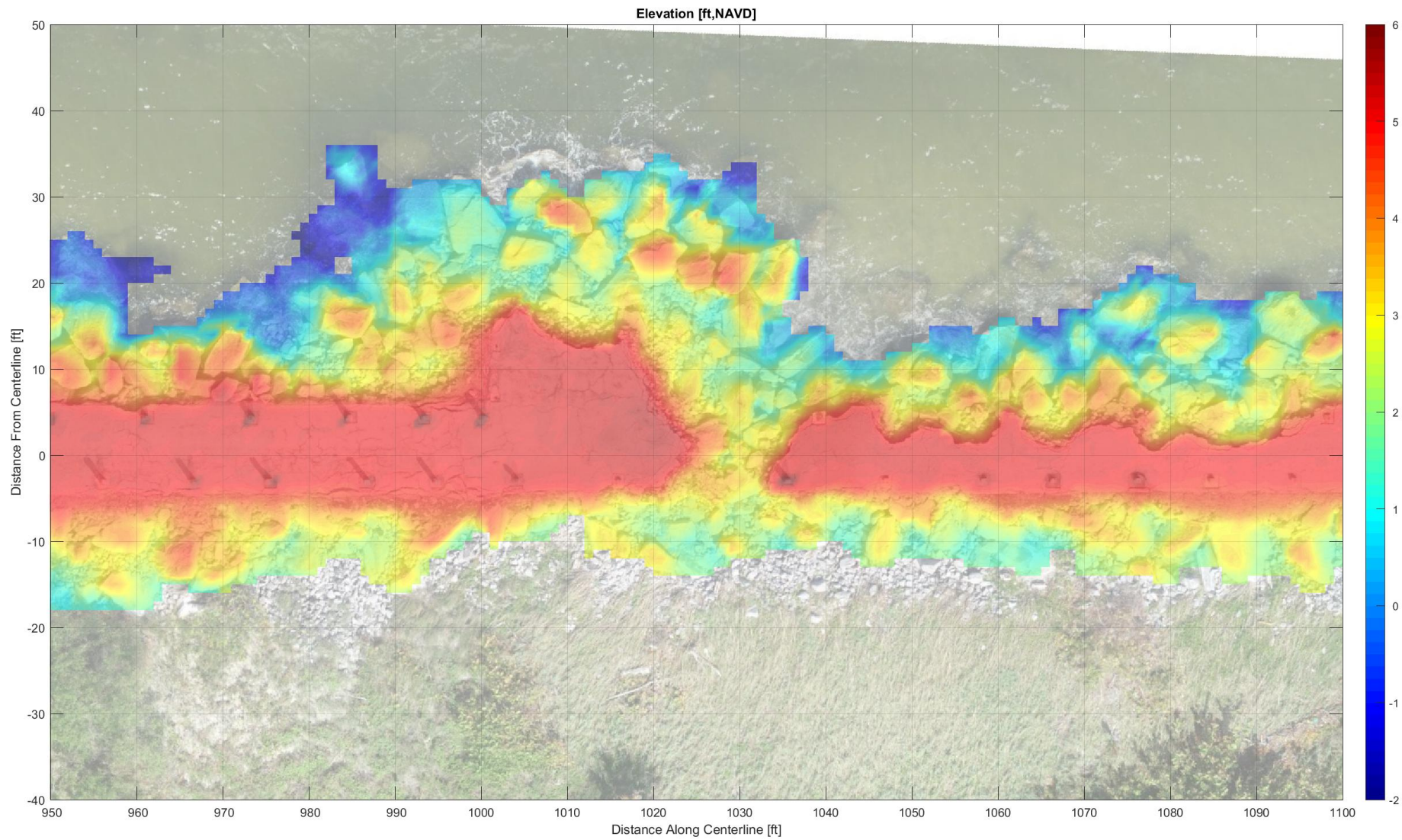


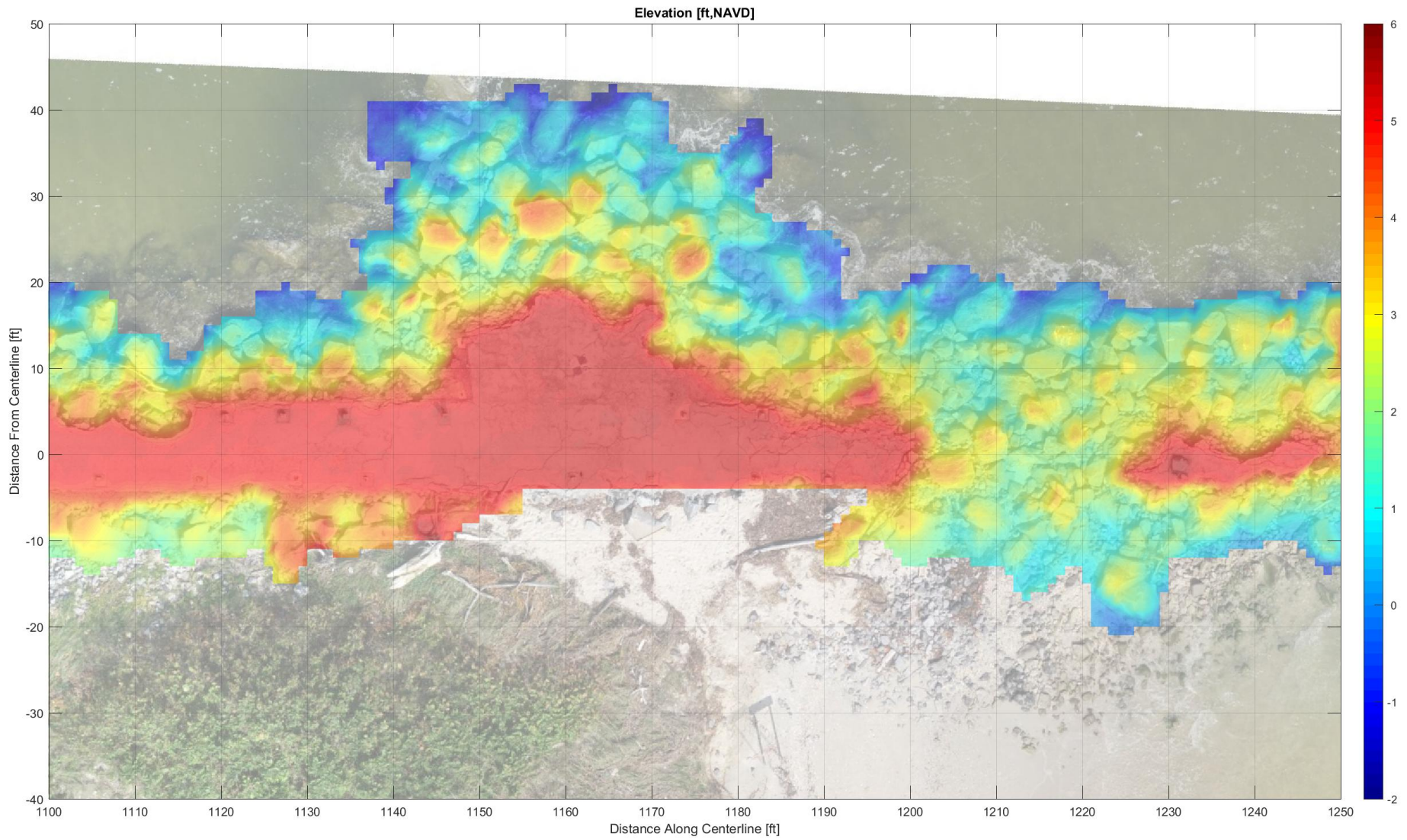


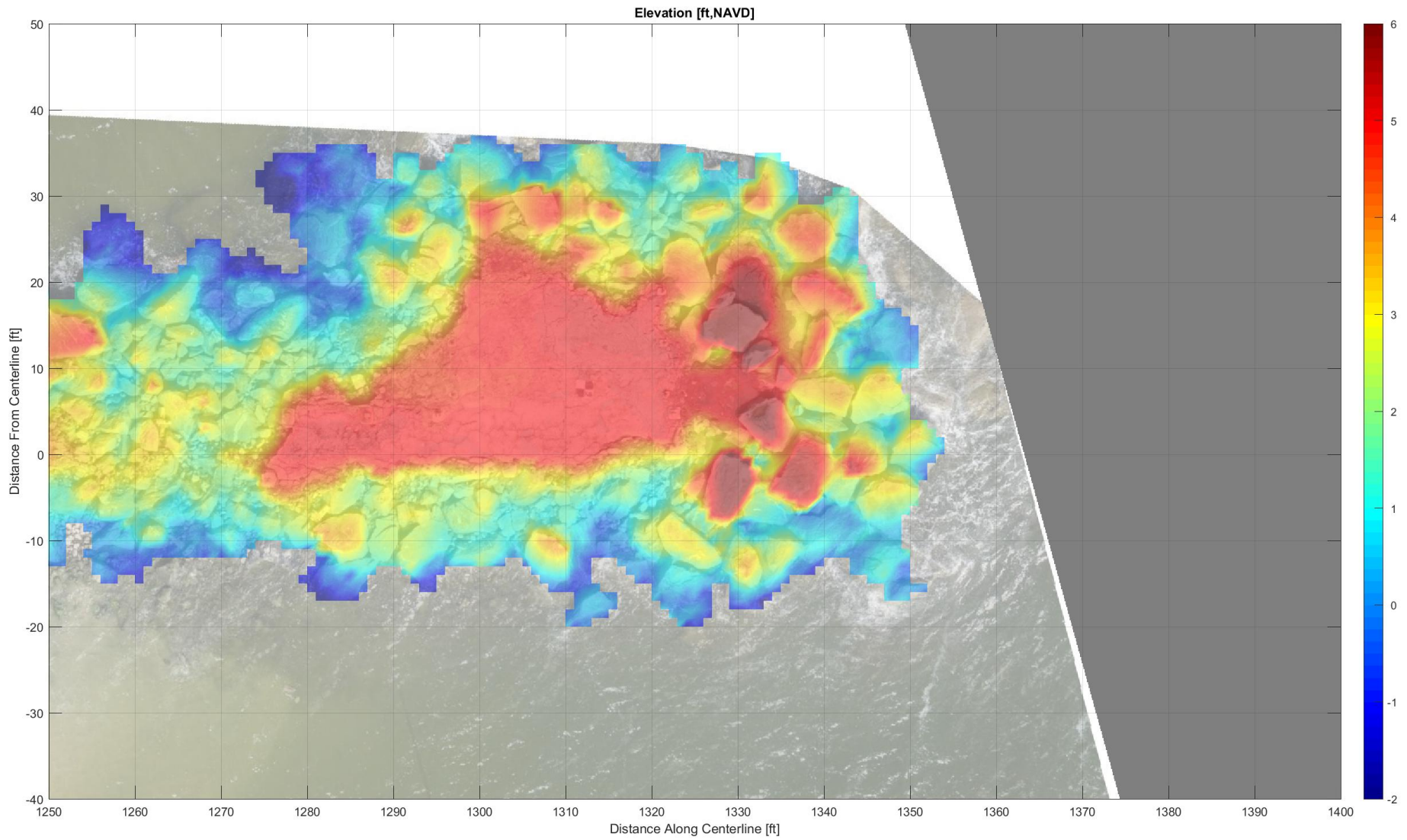




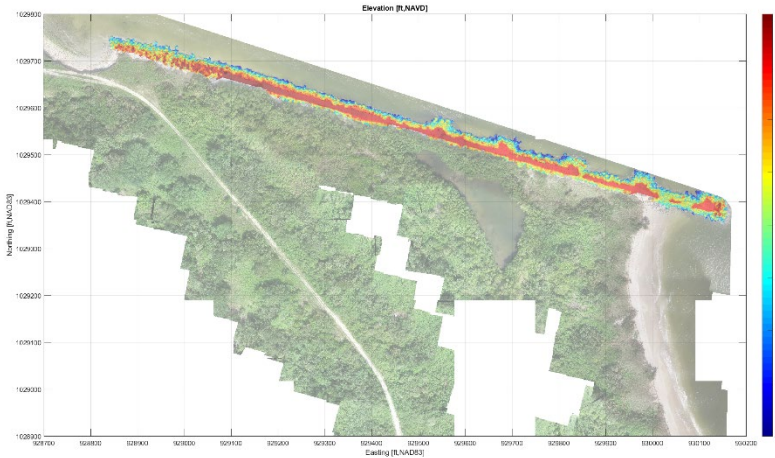








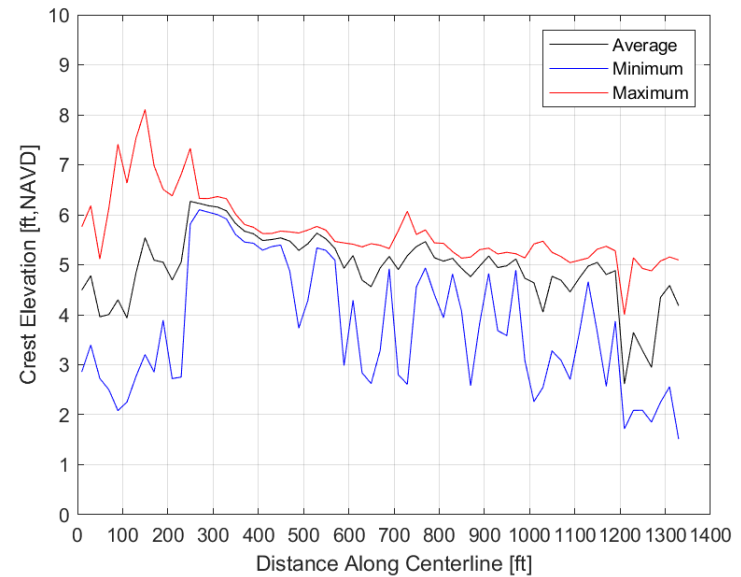
# JETTY CREST ELEVATION



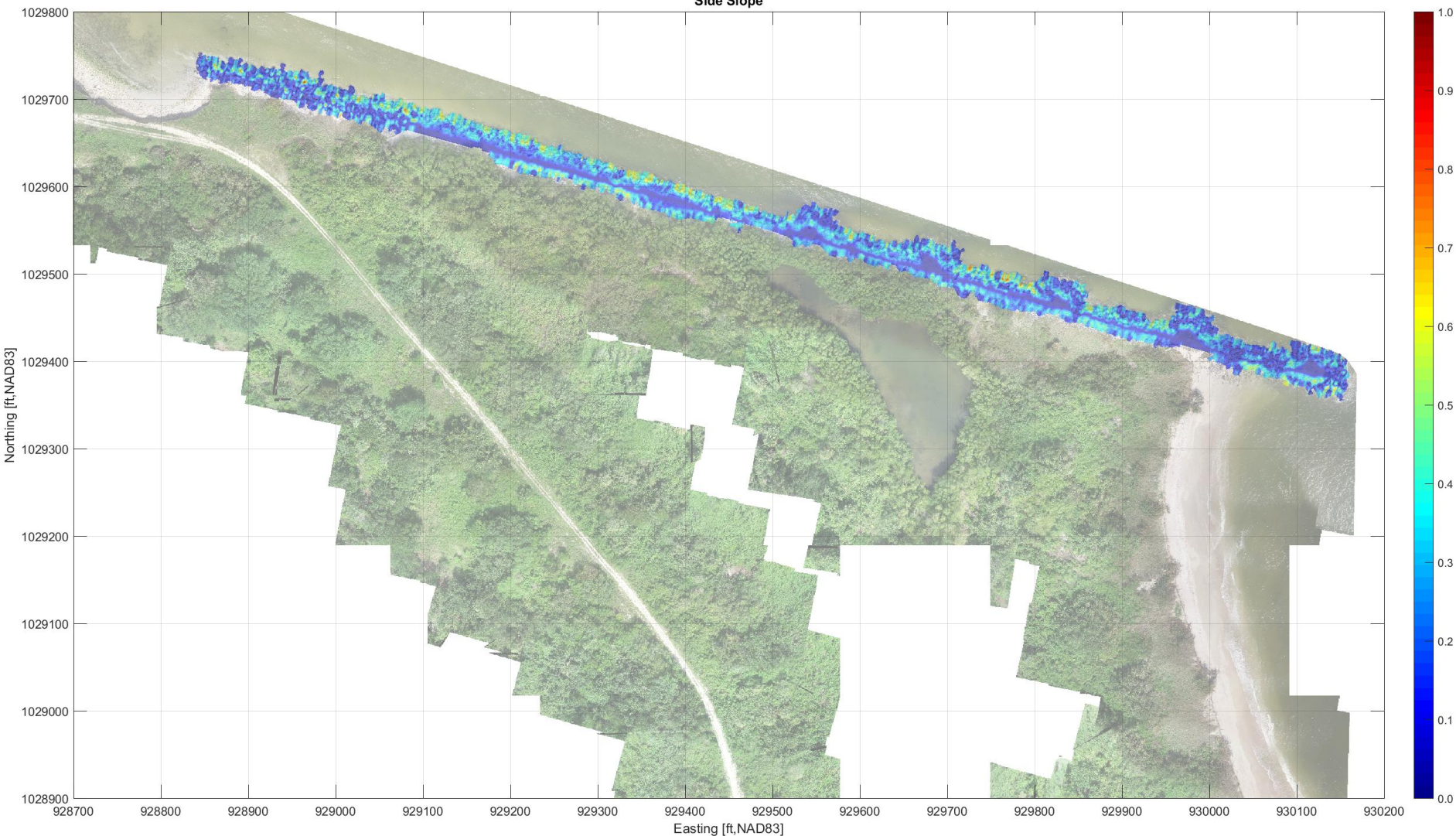
› Minimum, maximum, and average crest elevations were calculated for each 20-foot segment along the jetty.

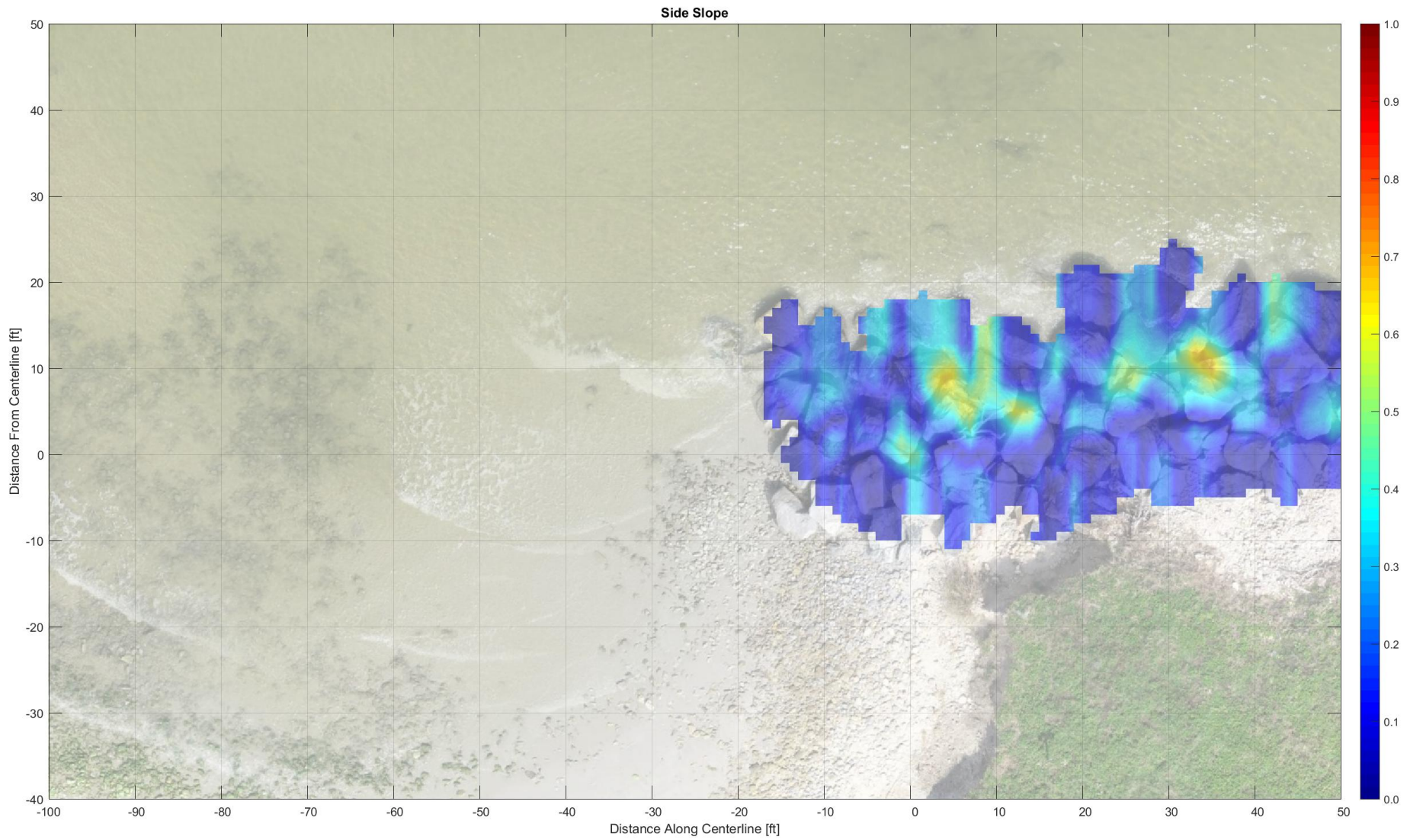
## › Crest Elevation (ft,NAVD)

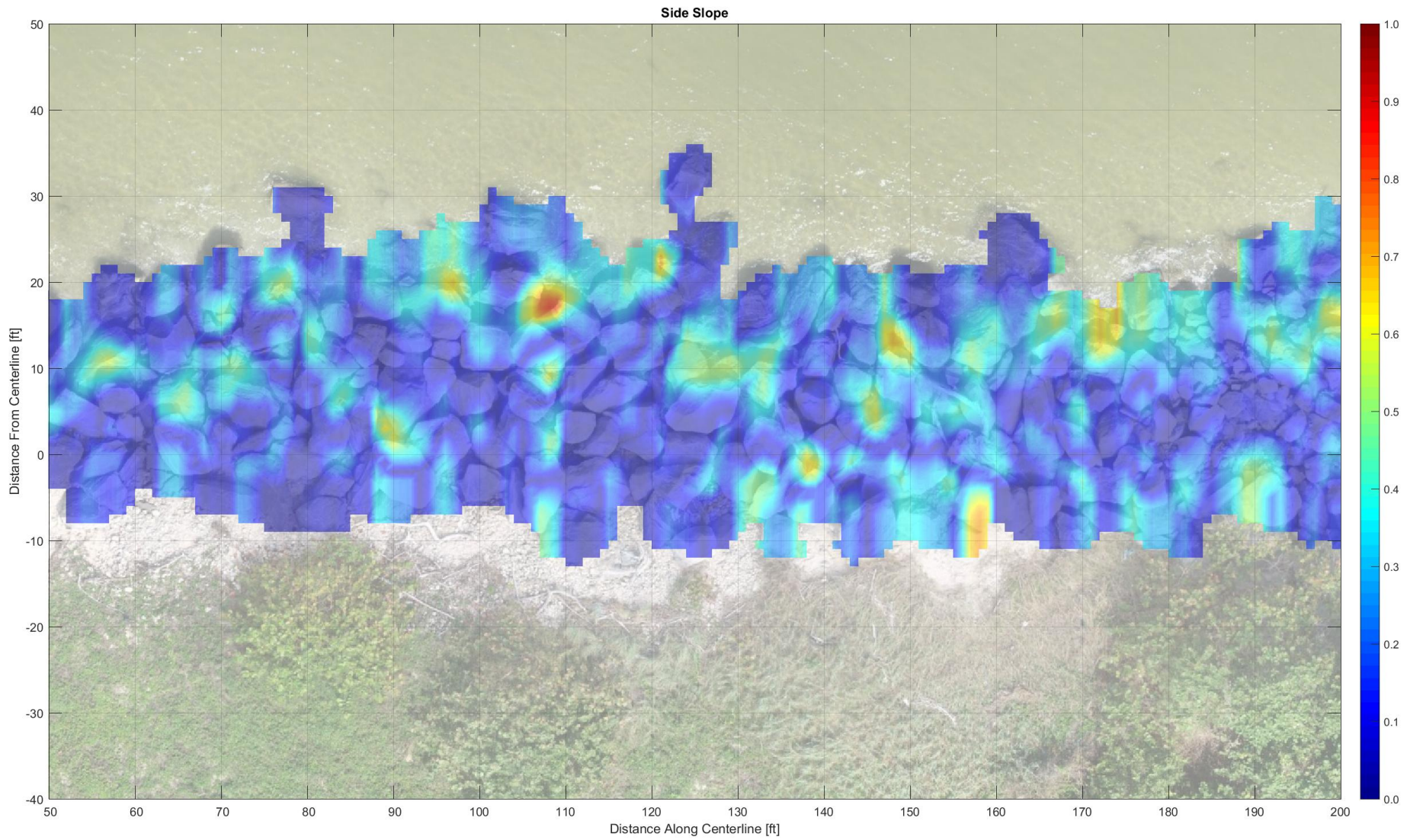
Face	Min	Max	Avg
Crest	1.5	8.1	4.9

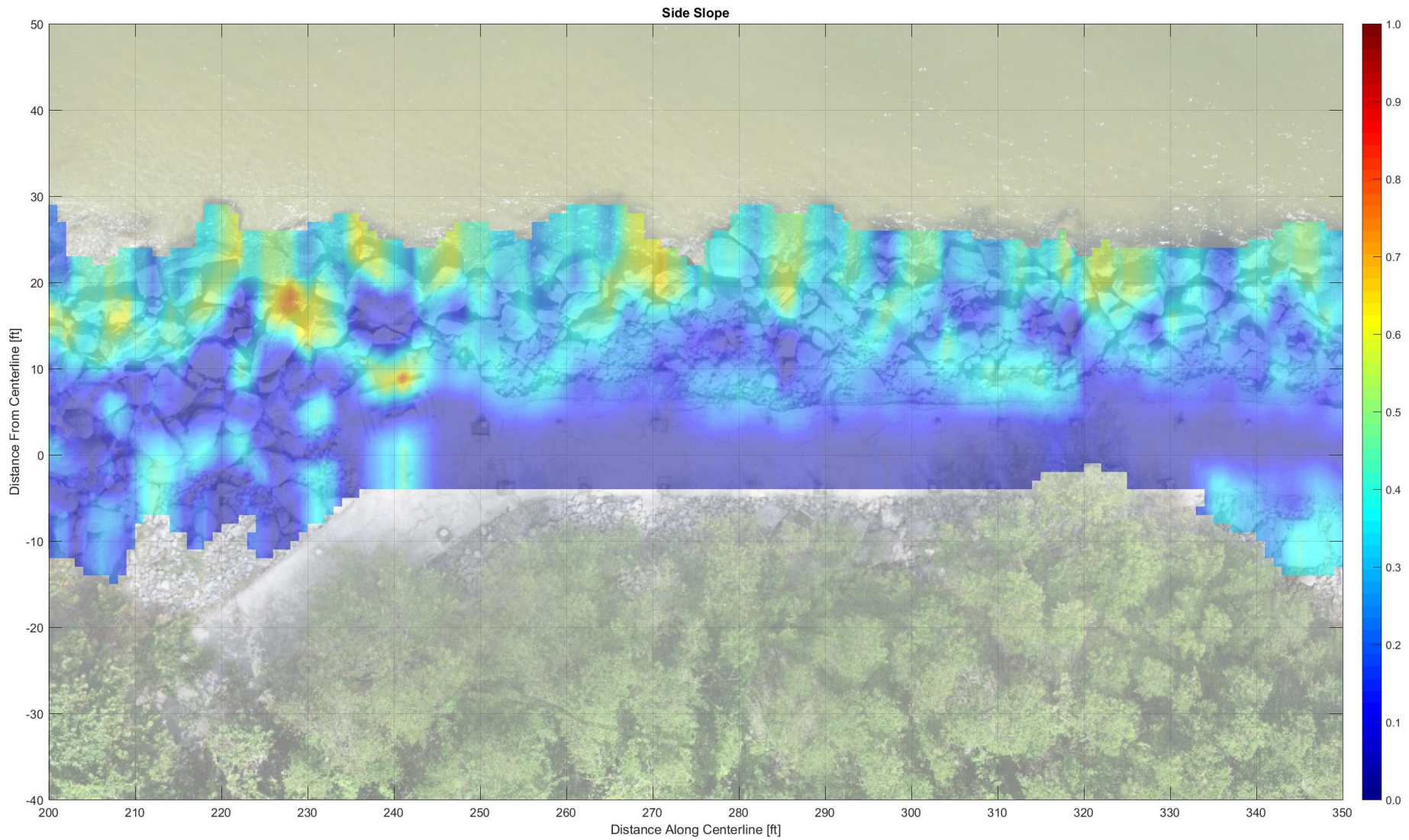


### Side Slope



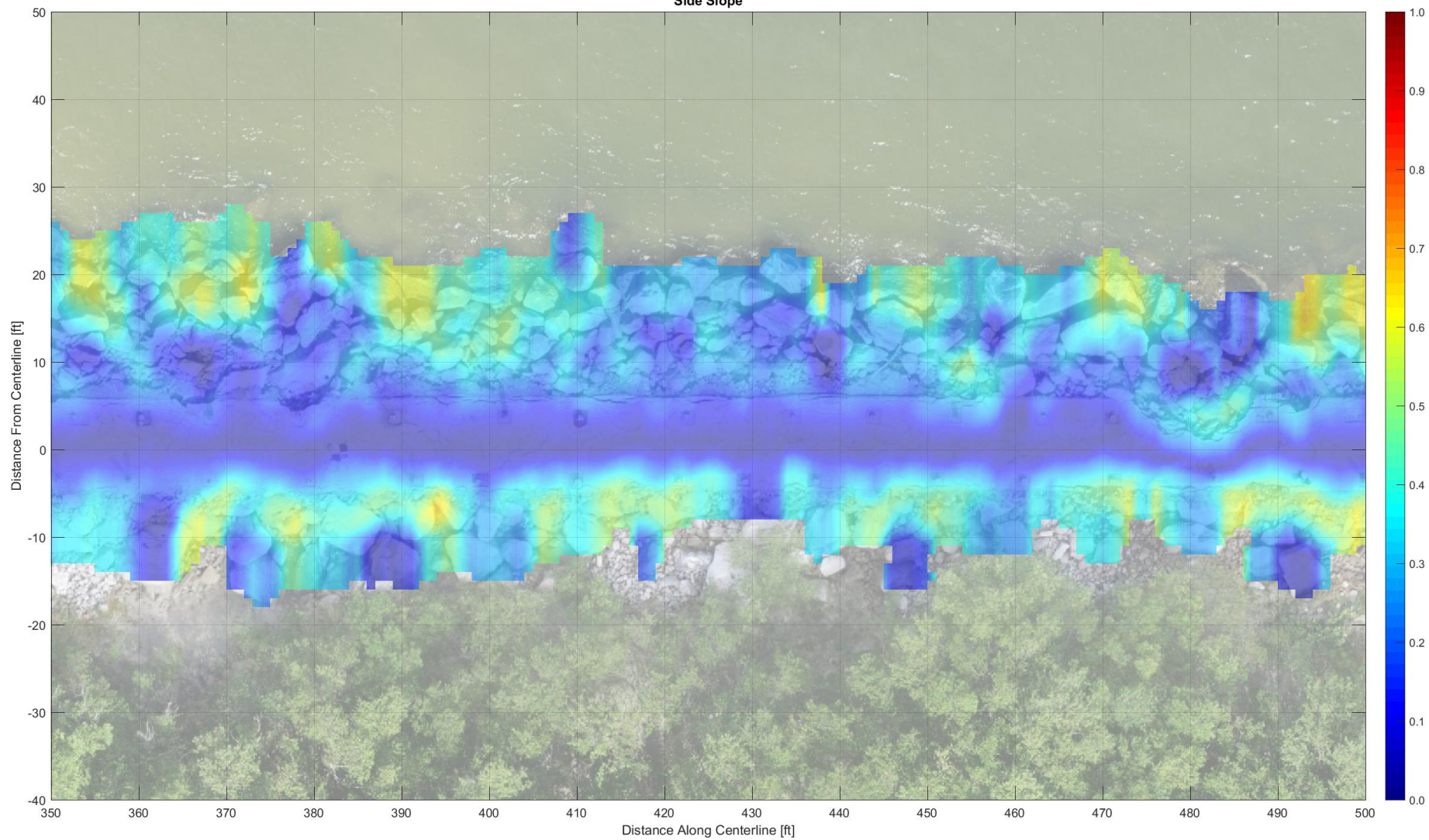


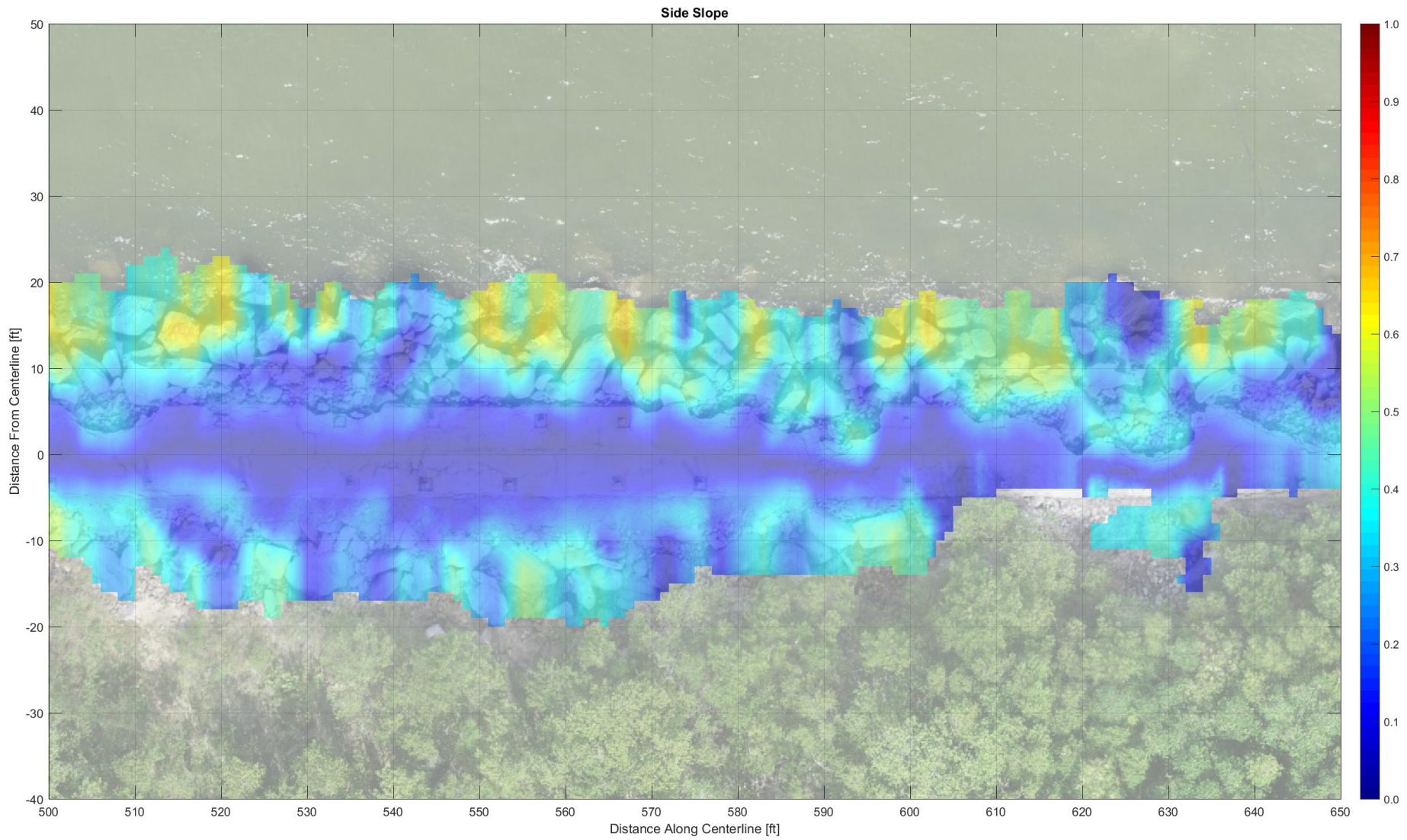


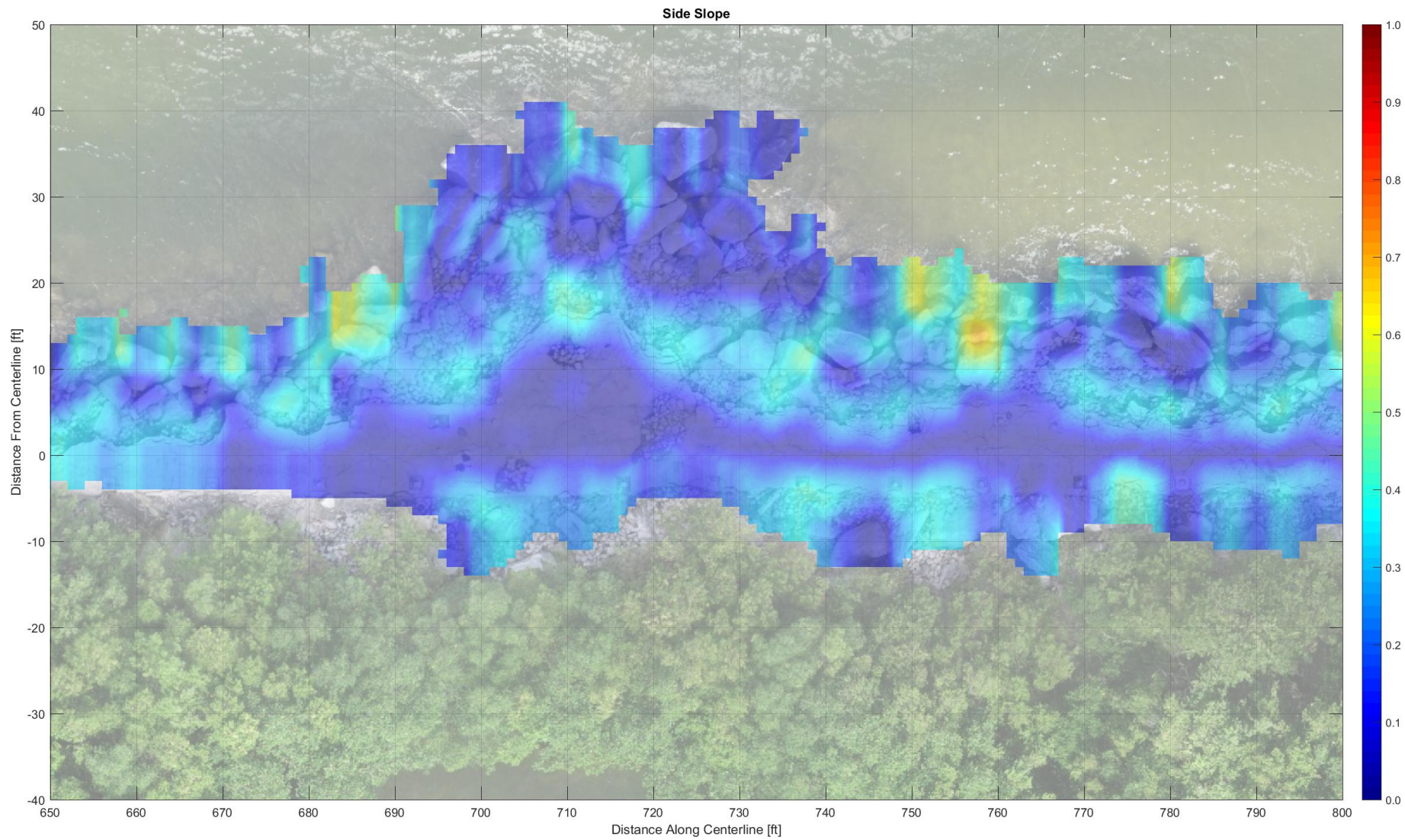


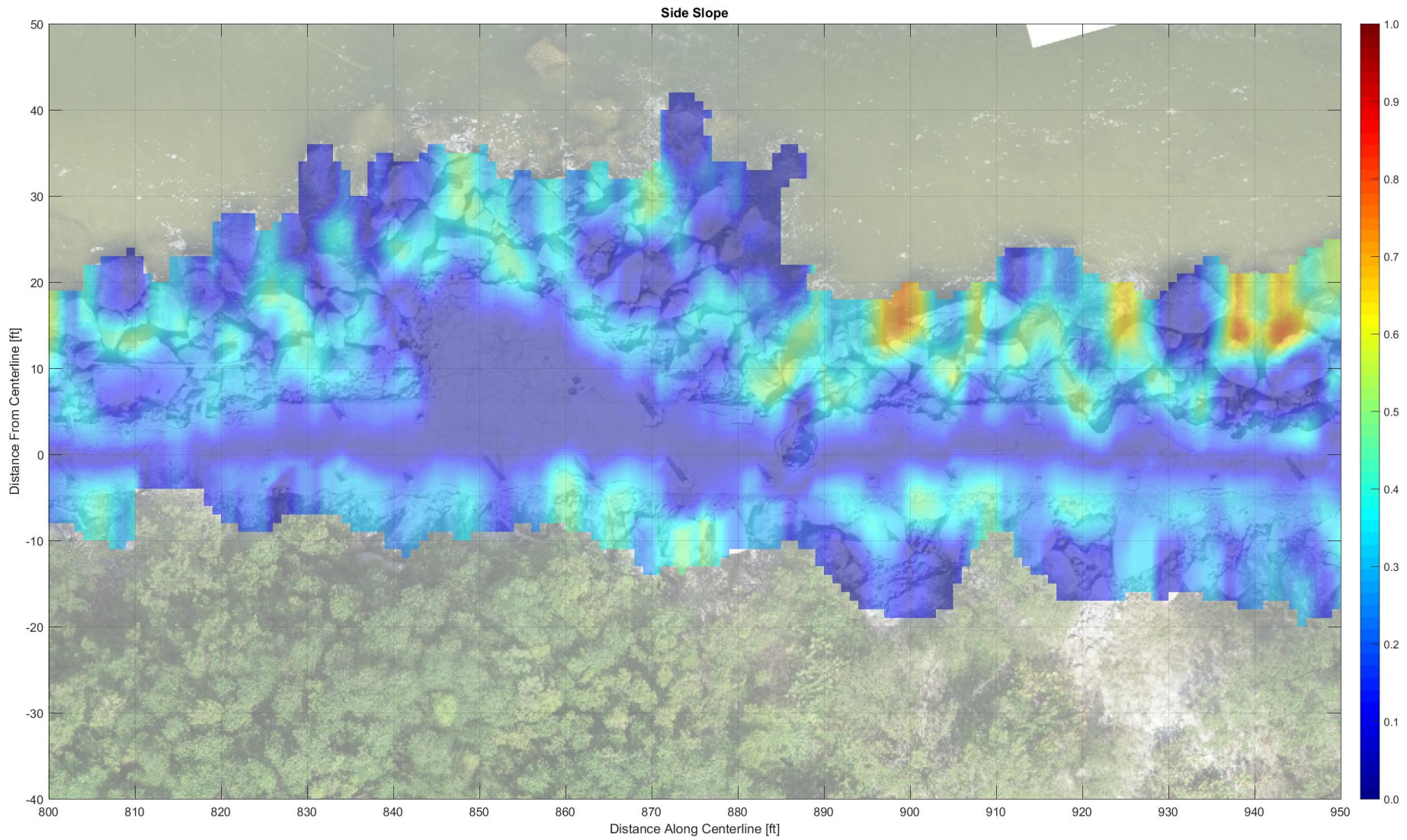


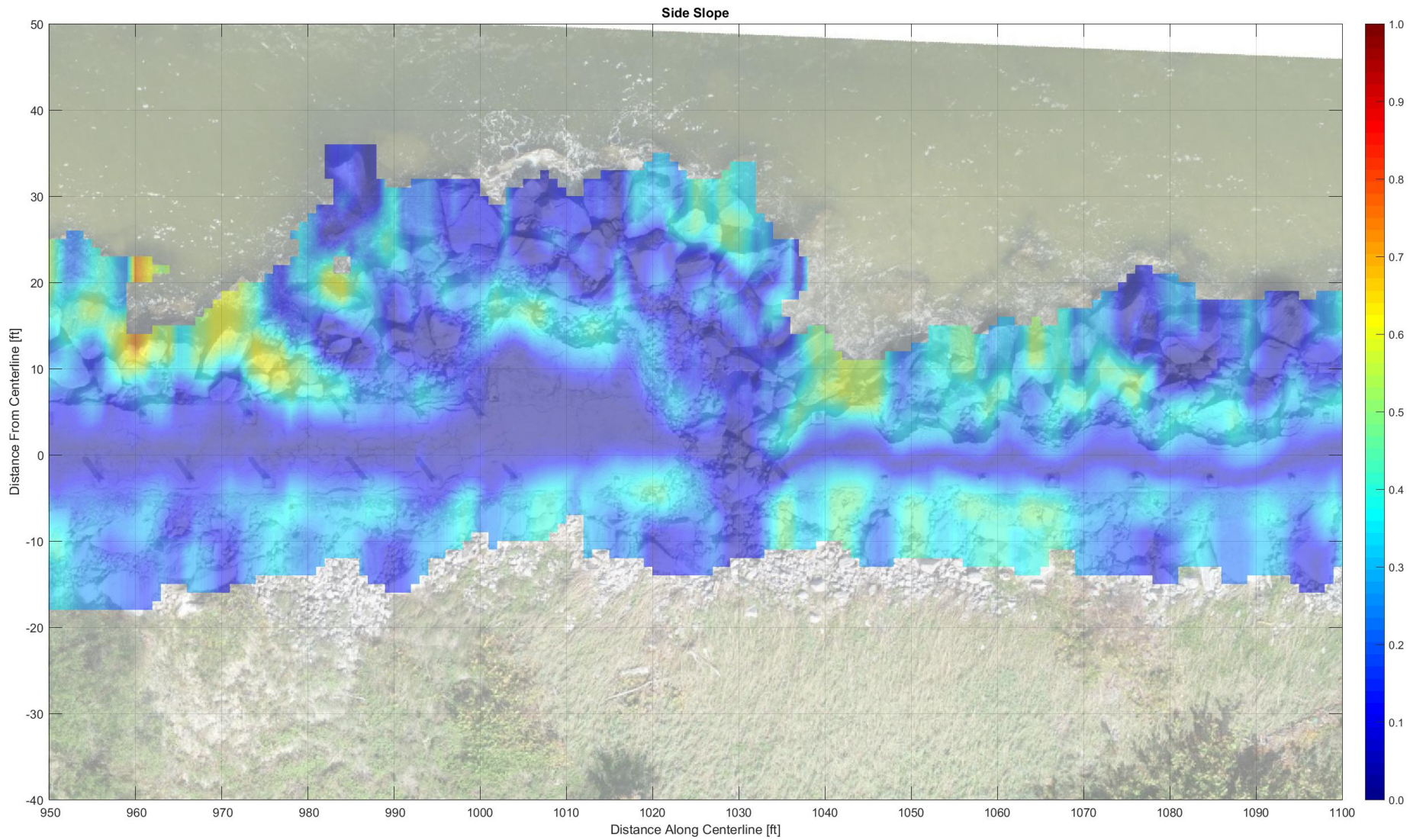
### Side Slope

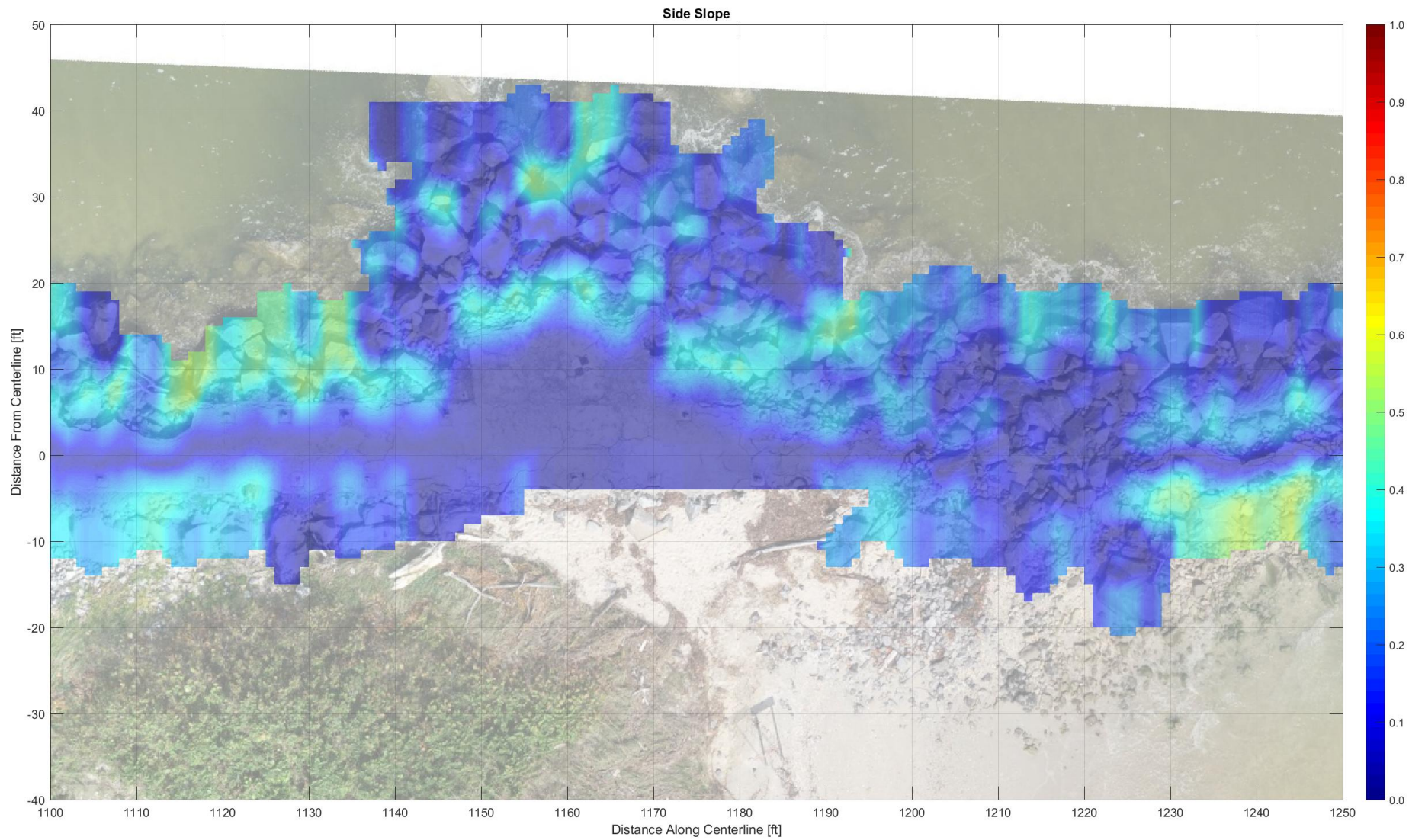


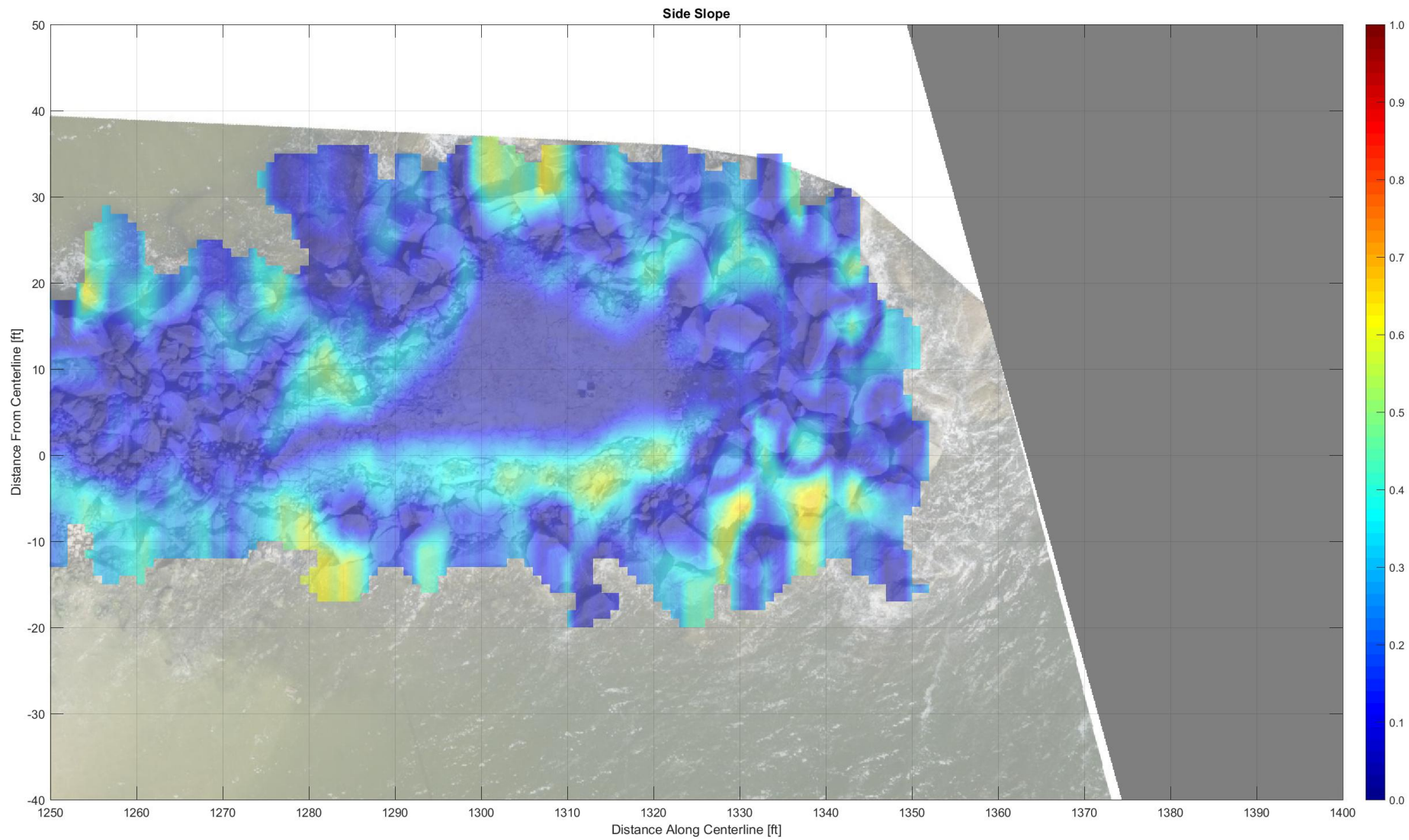




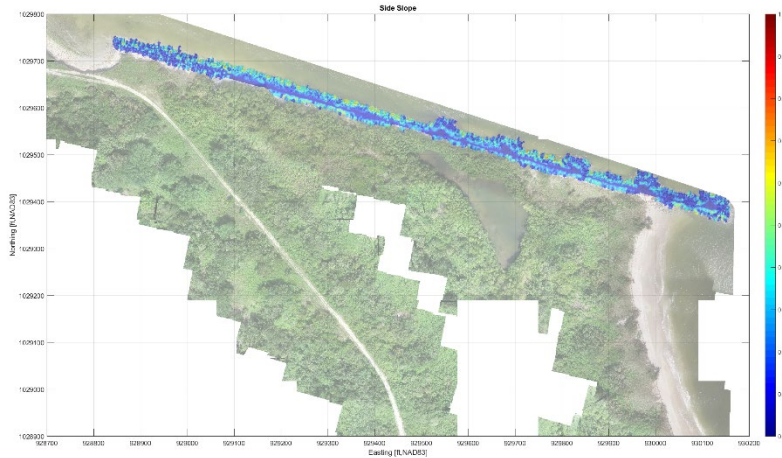








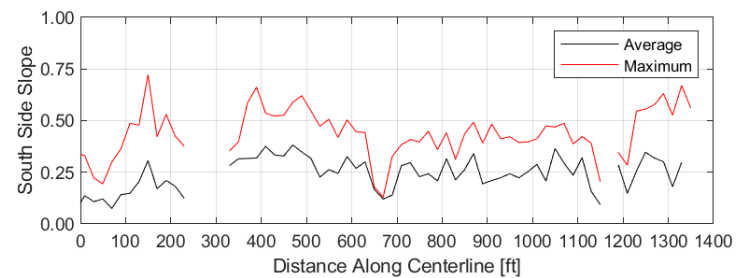
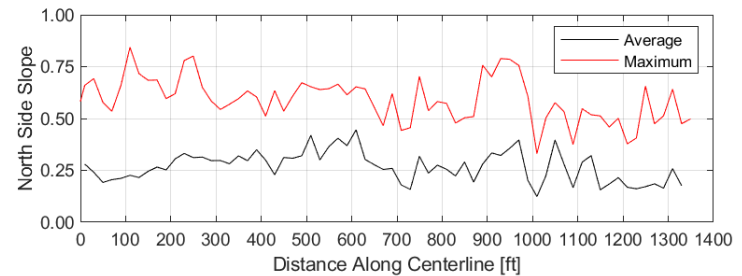
# JETTY SIDE SLOPES



## › Side Slope

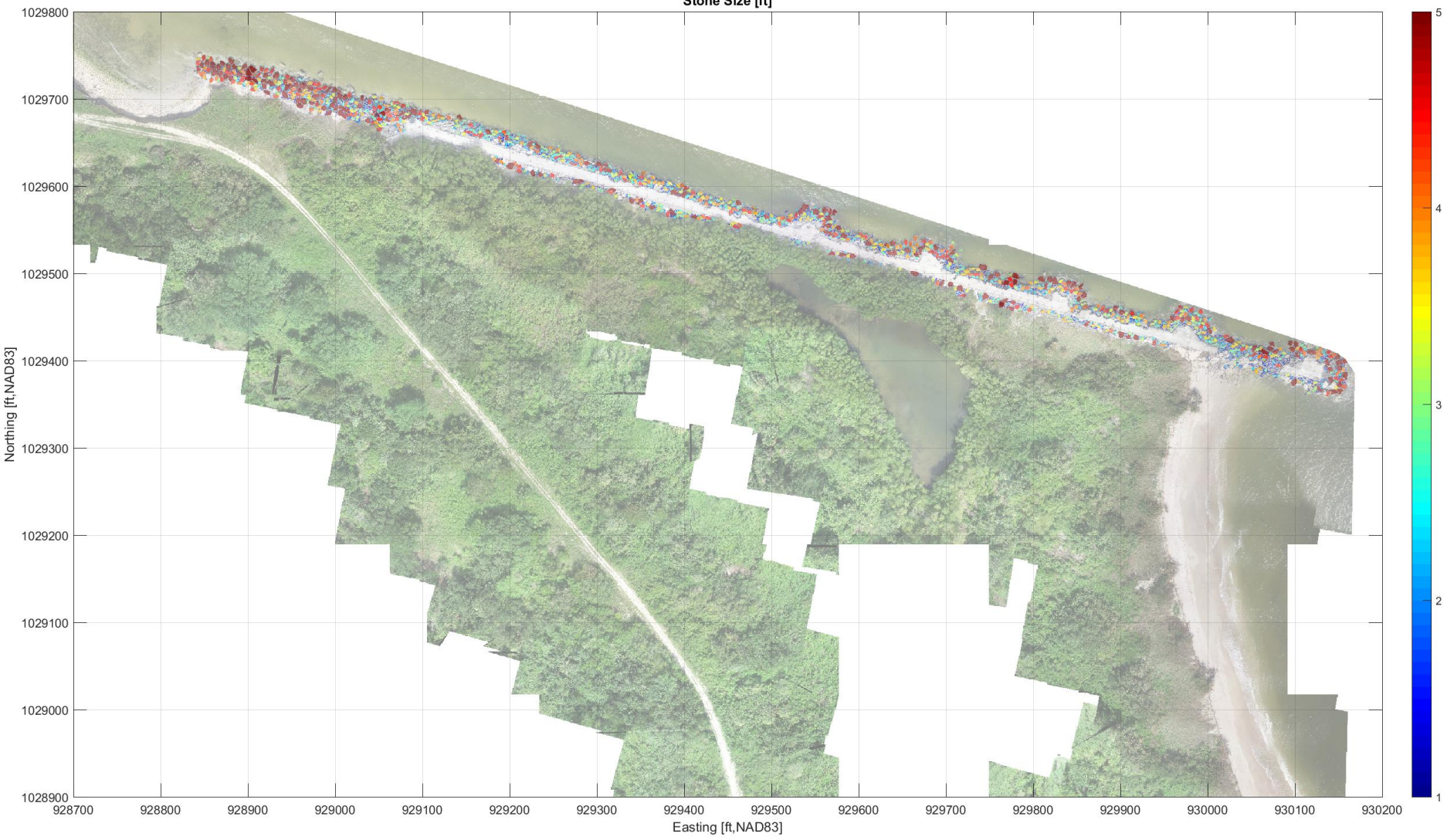
Face	Min	Max	Avg
North	1V:3.0H	1V:1.2H	1V:3.7H
South	1V:7.7H	1V:1.4H	1V:4.1H

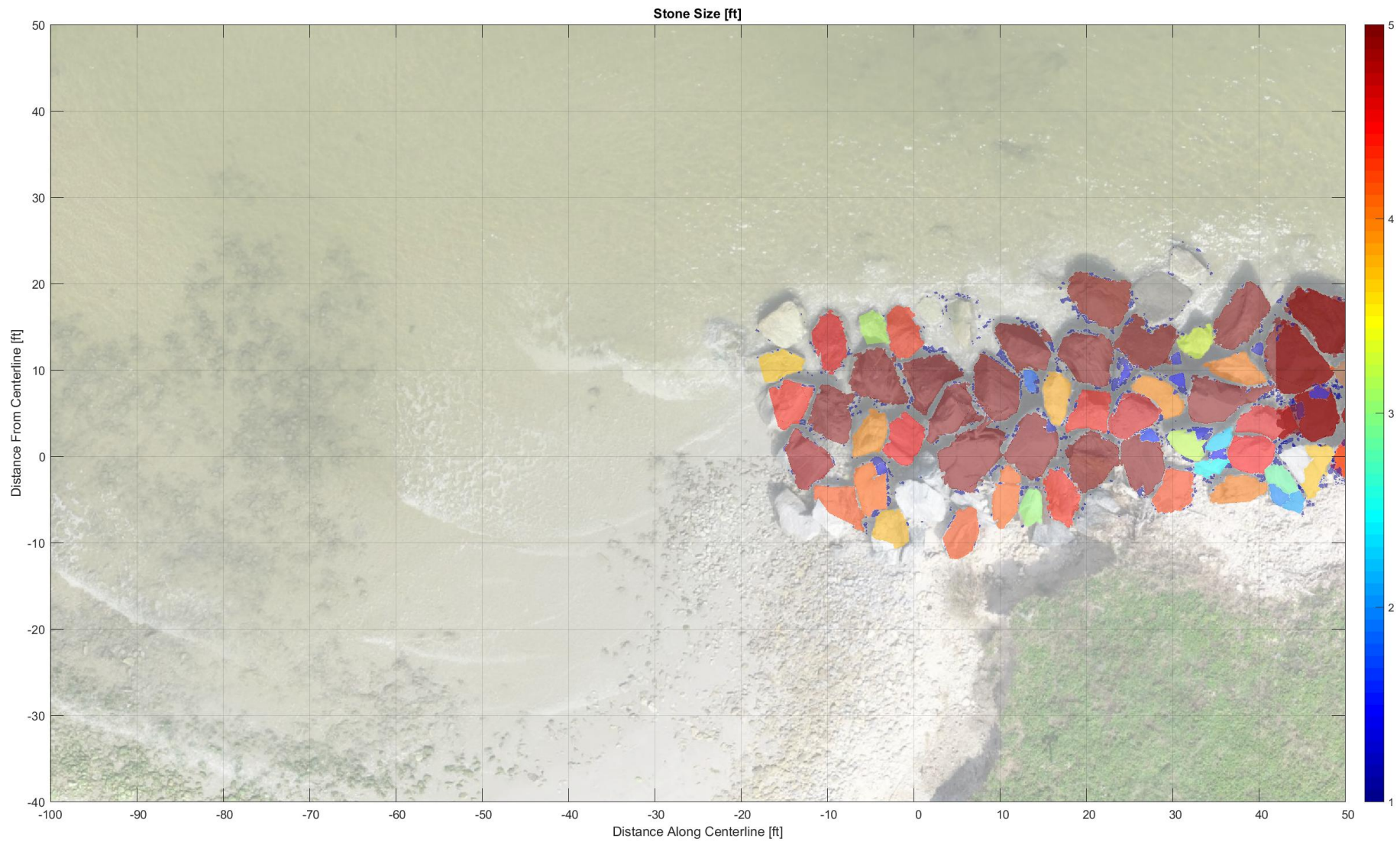
› Average and maximum side slopes were calculated for each 20-foot segment along the north and south jetty faces.

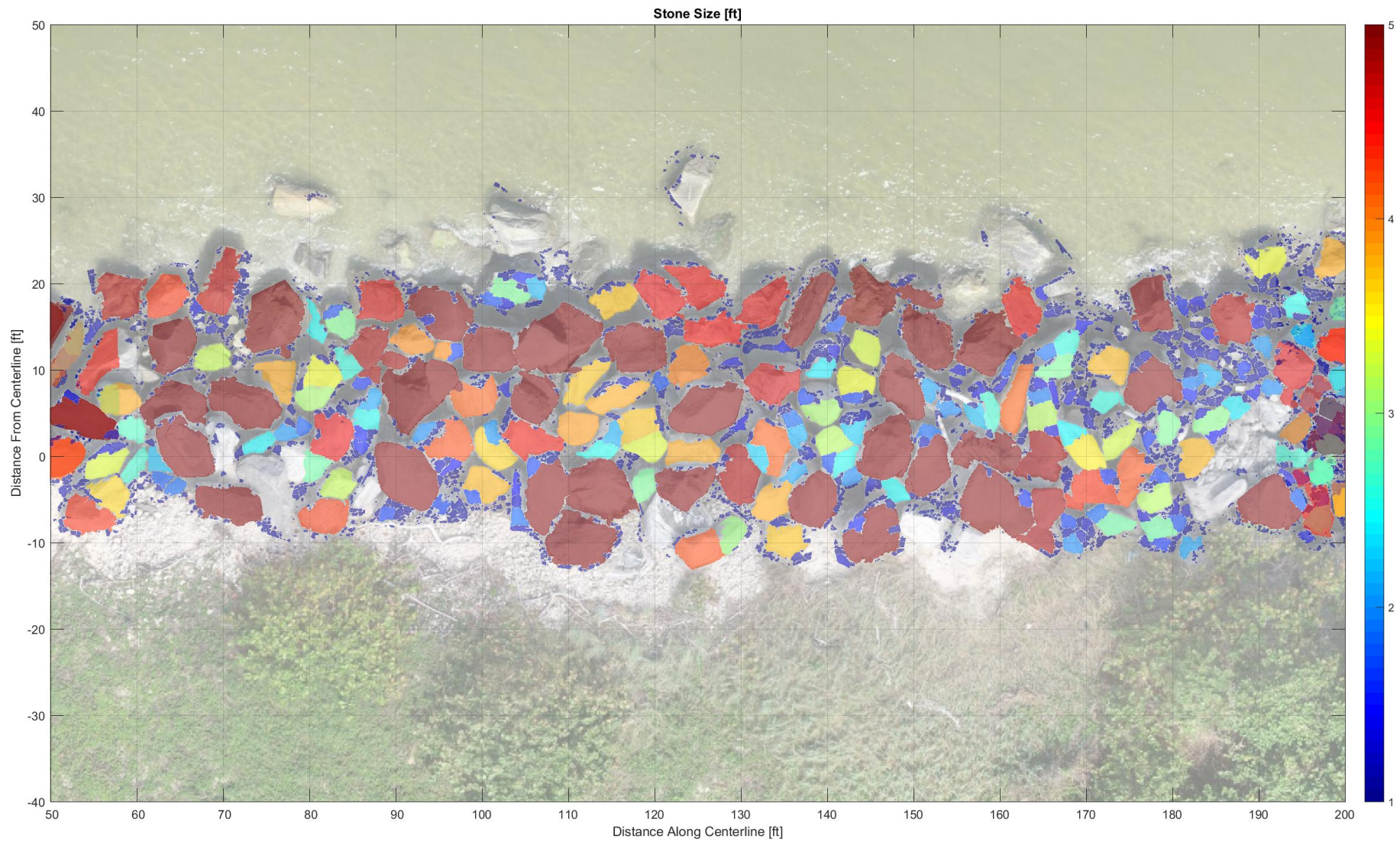


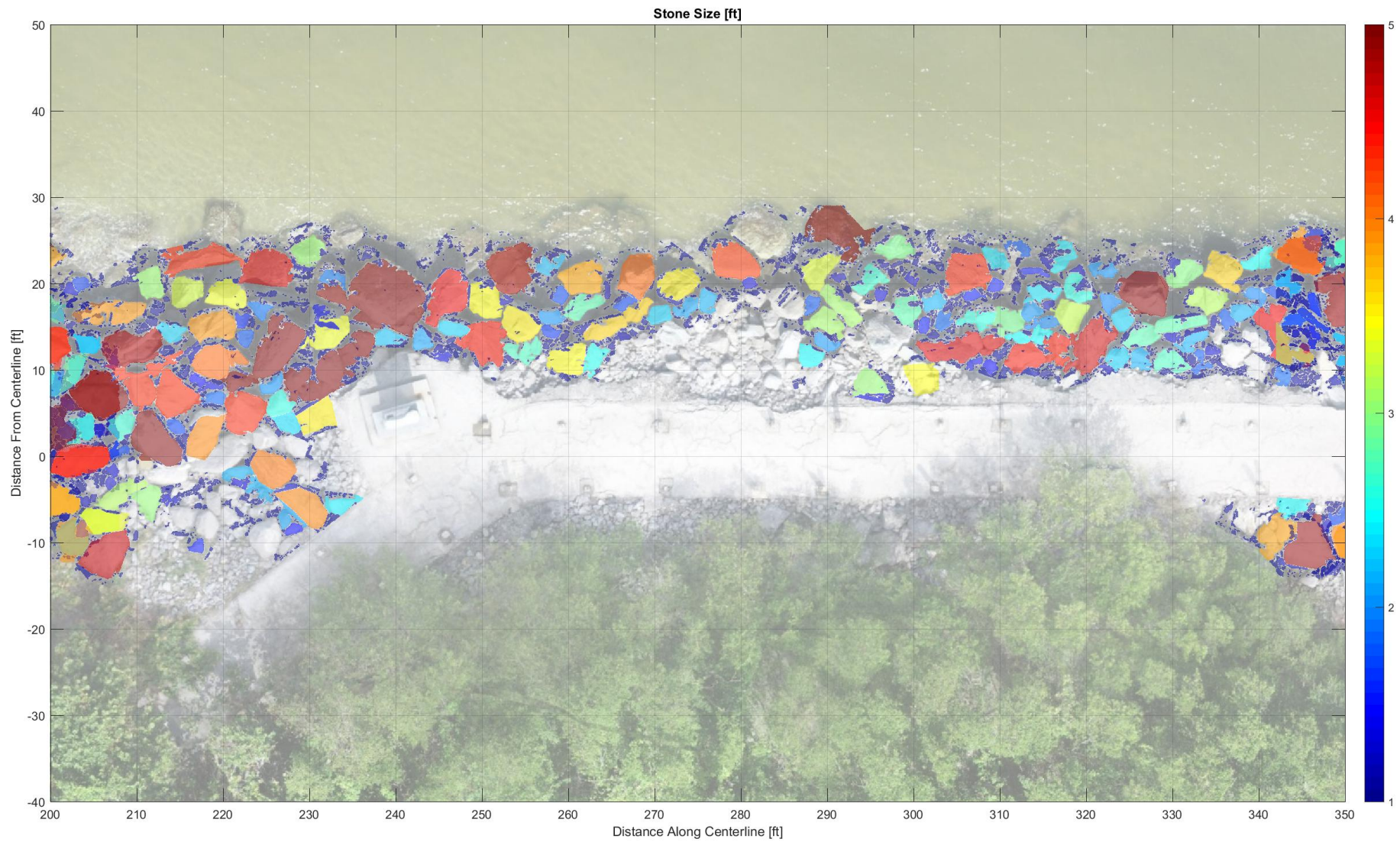


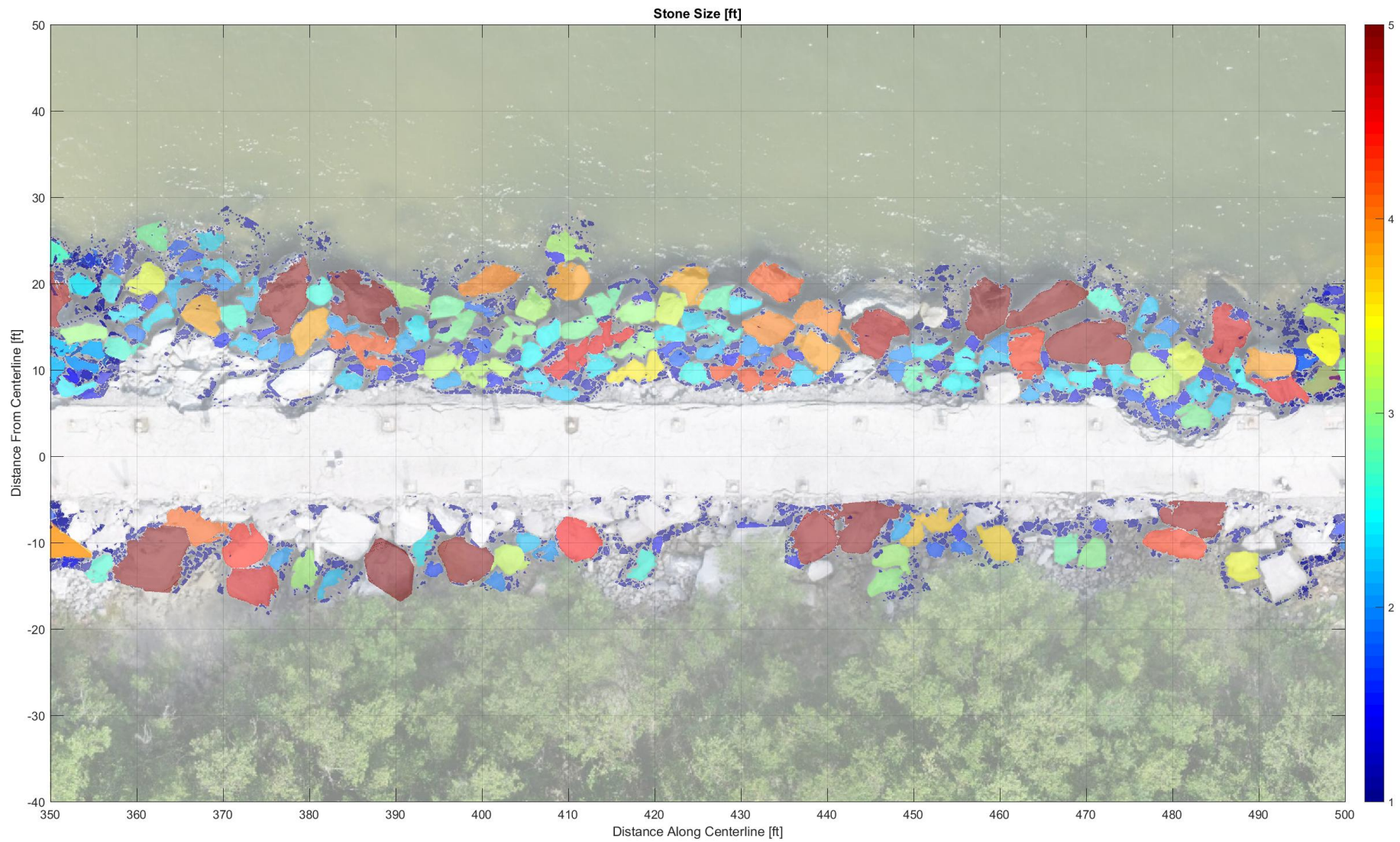
Stone Size [ft]

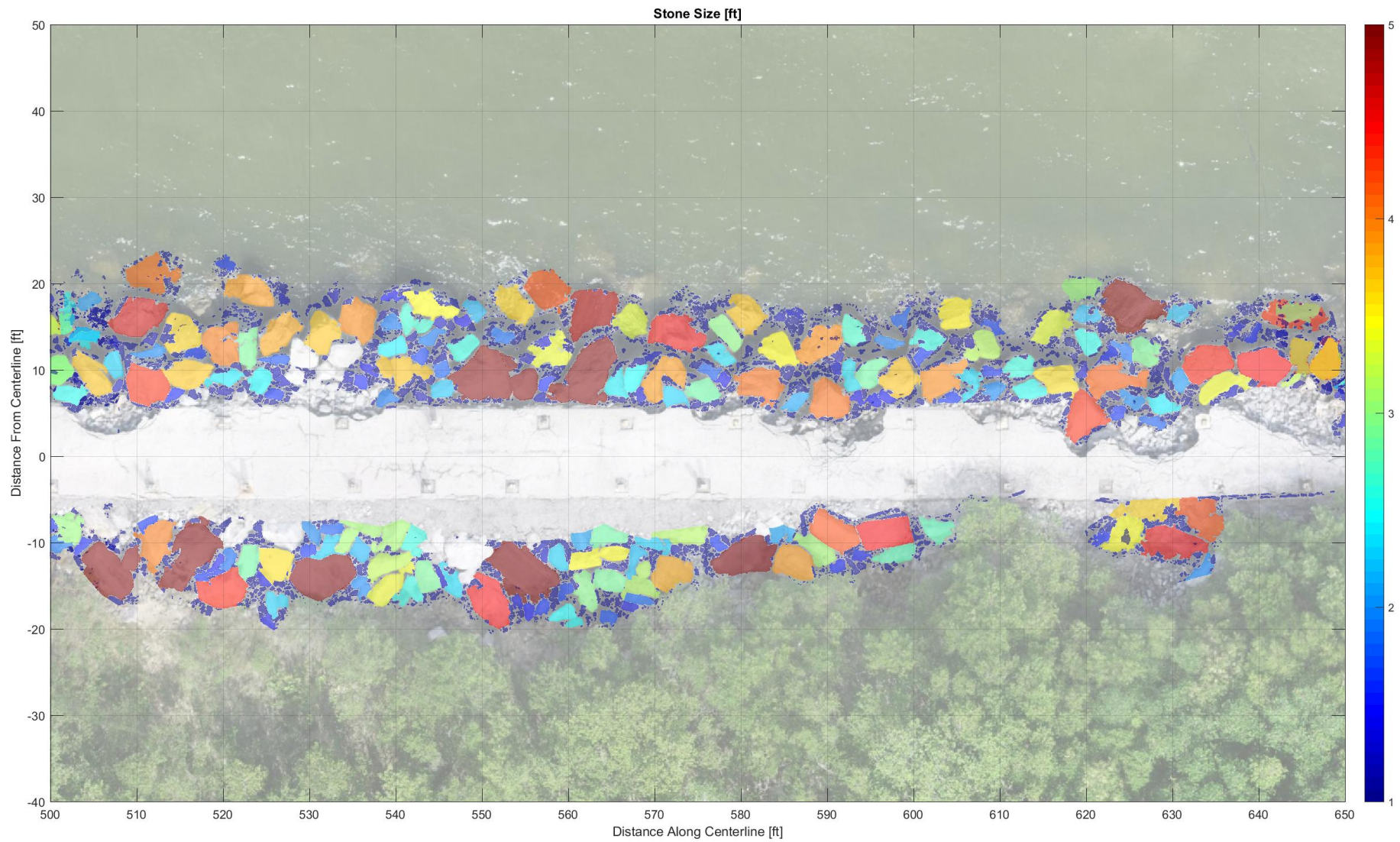


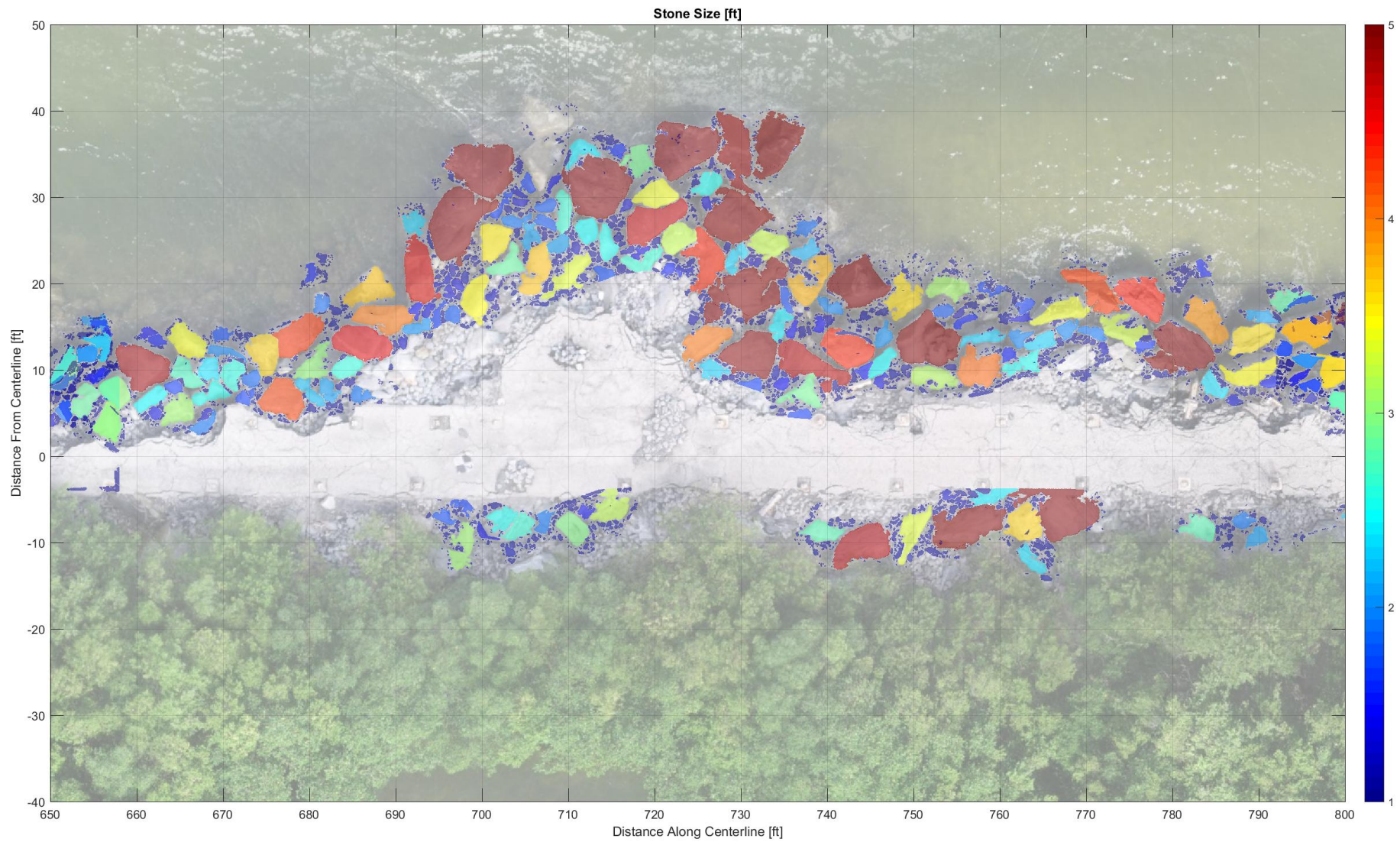


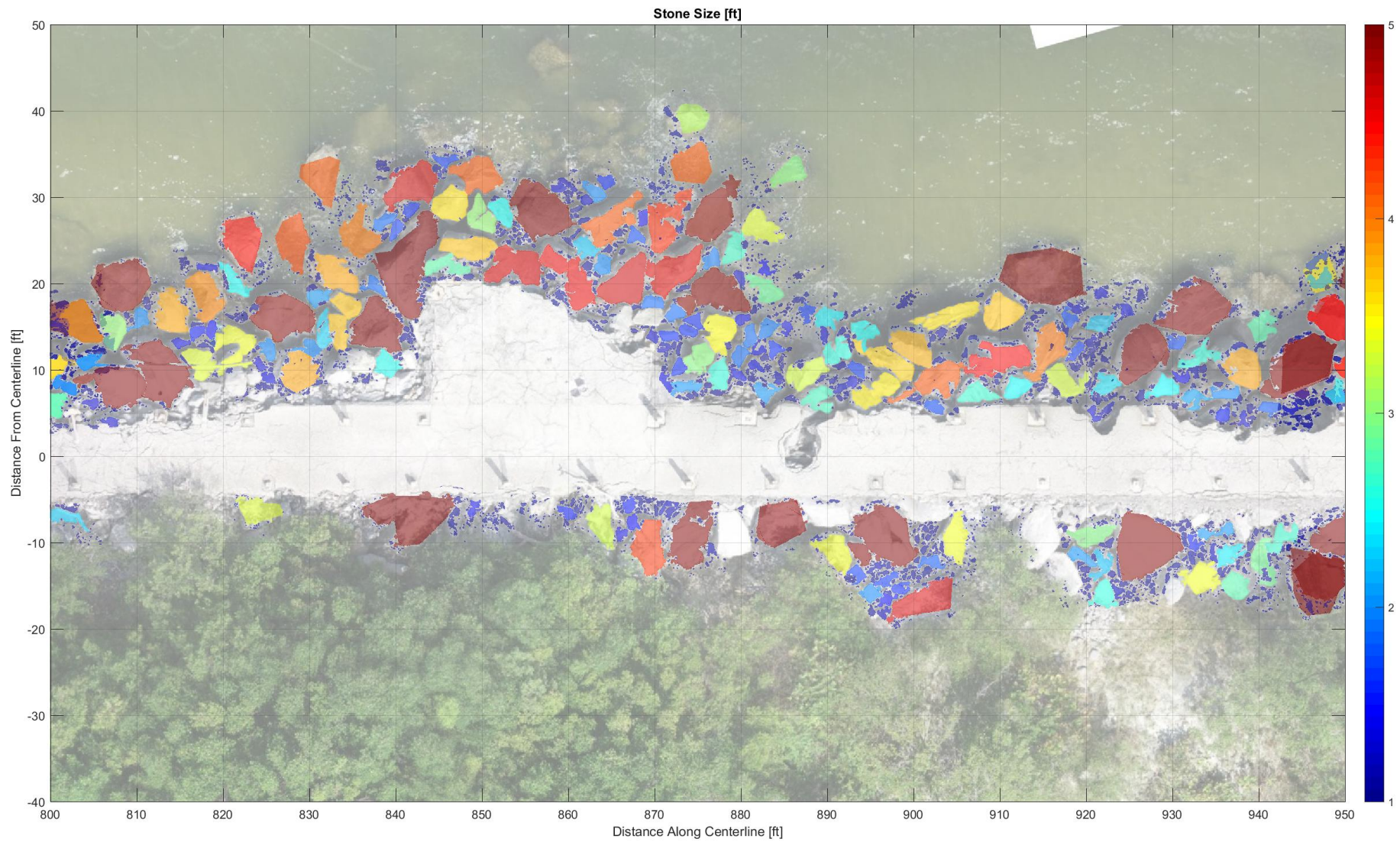




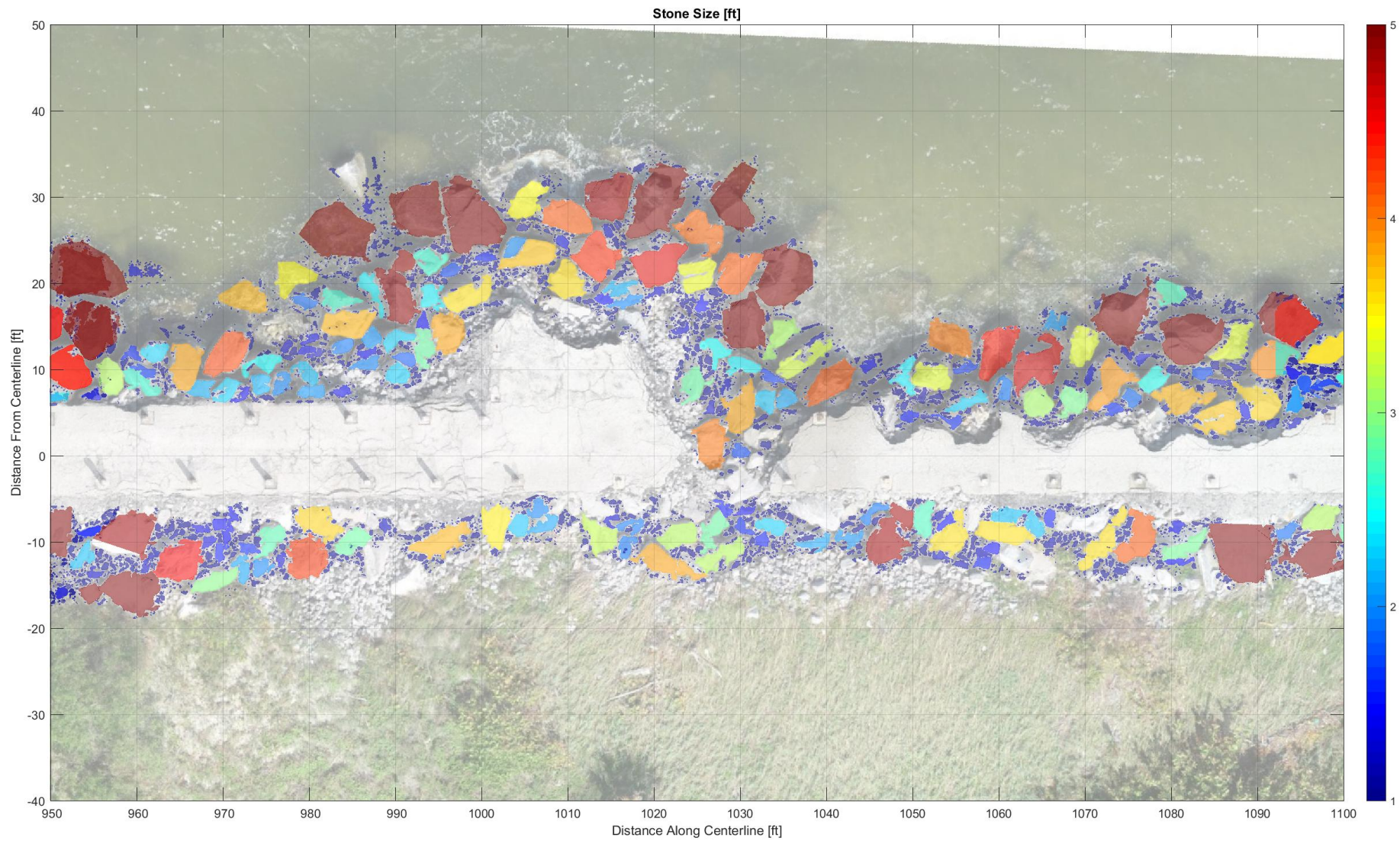


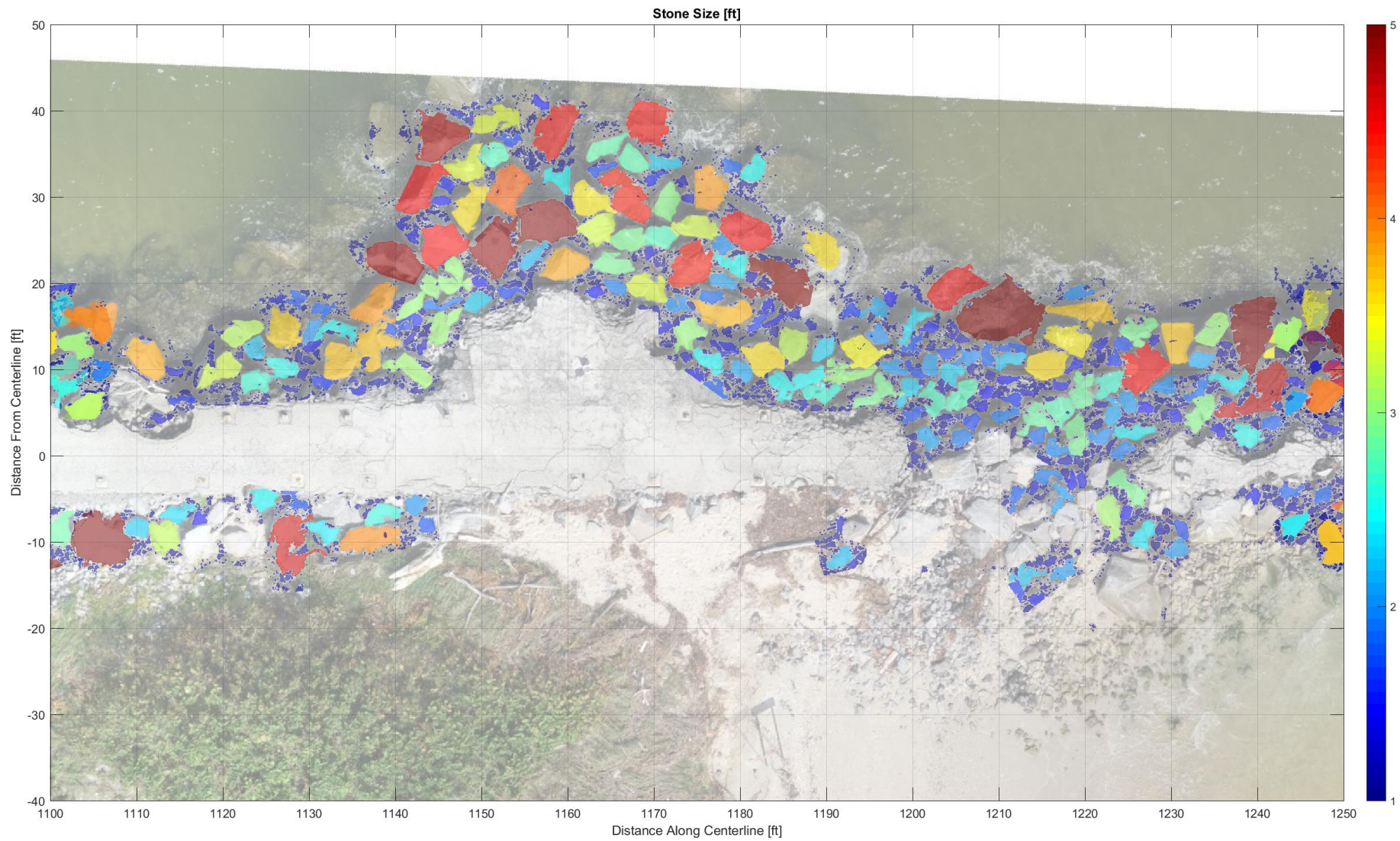


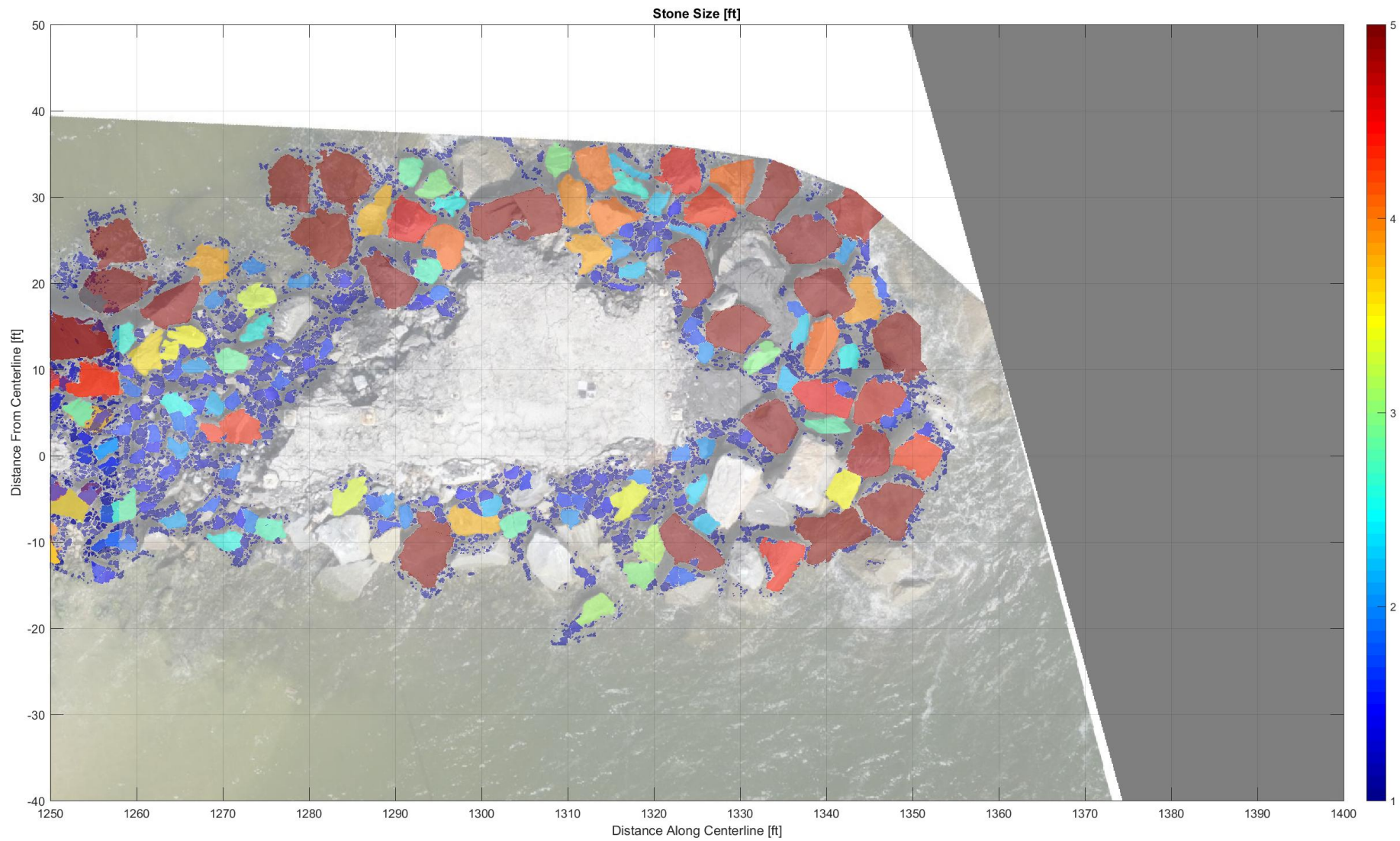




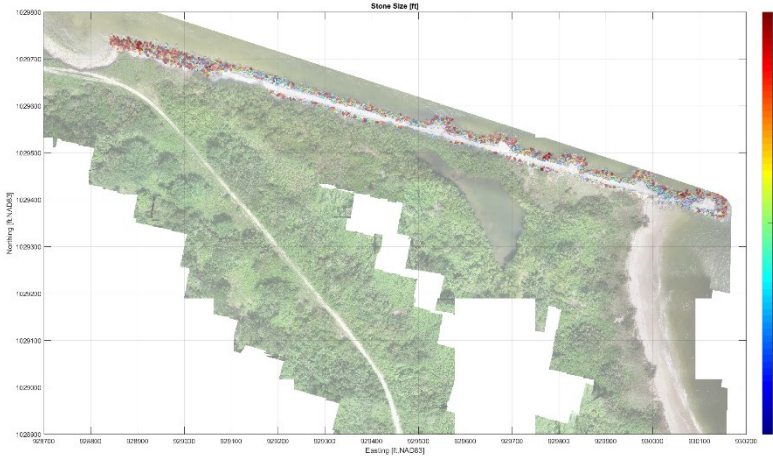








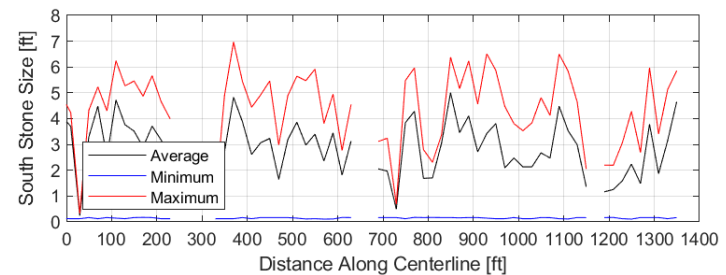
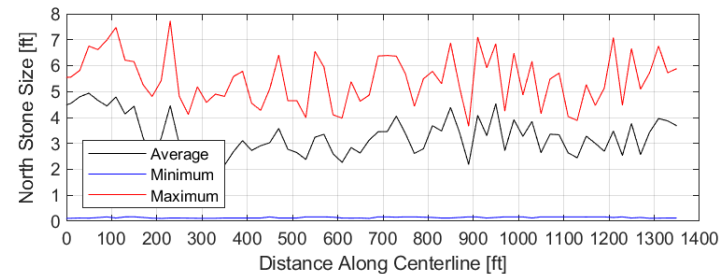
# JETTY STONE SIZES



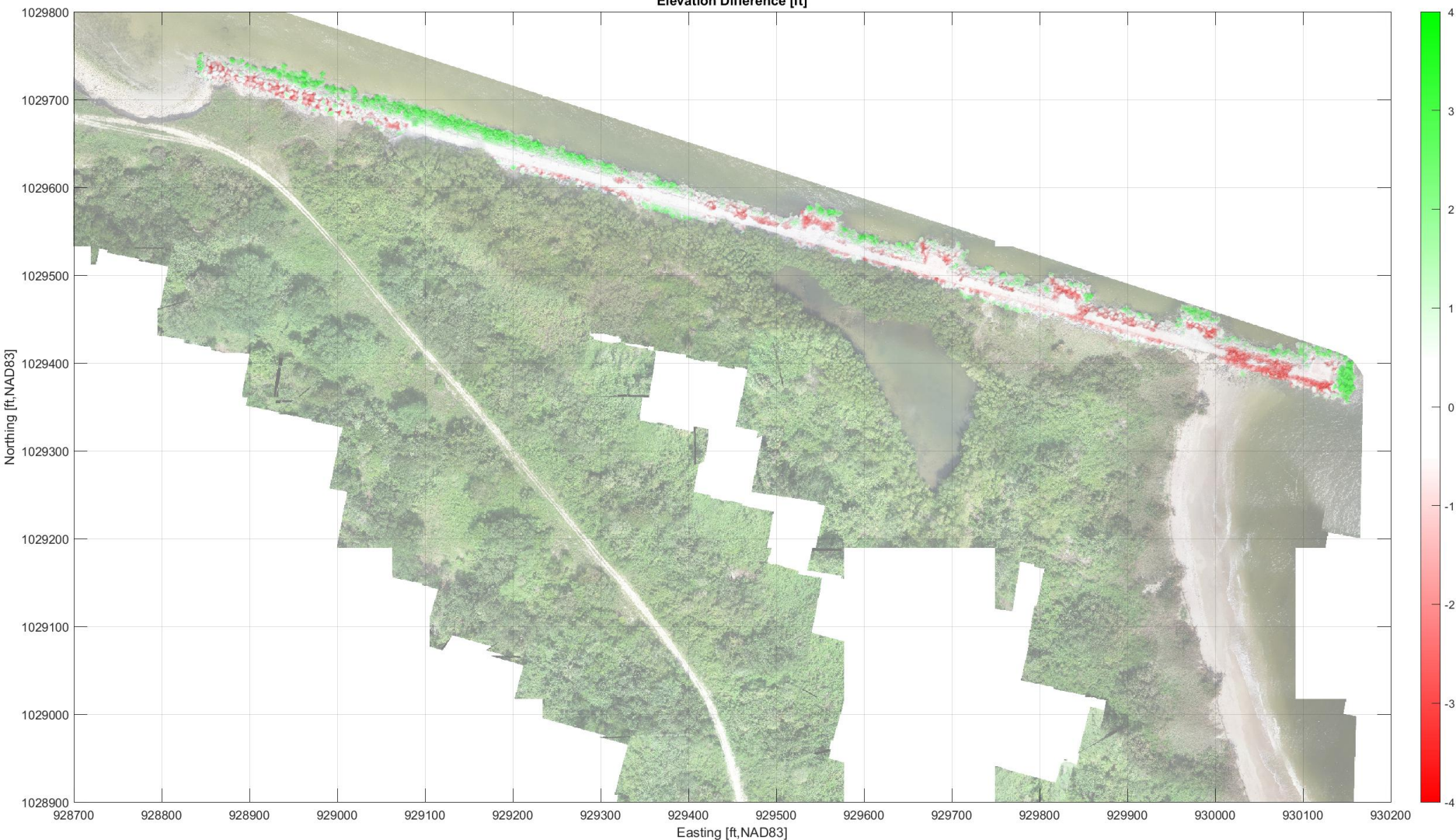
## Stone Size (ft)

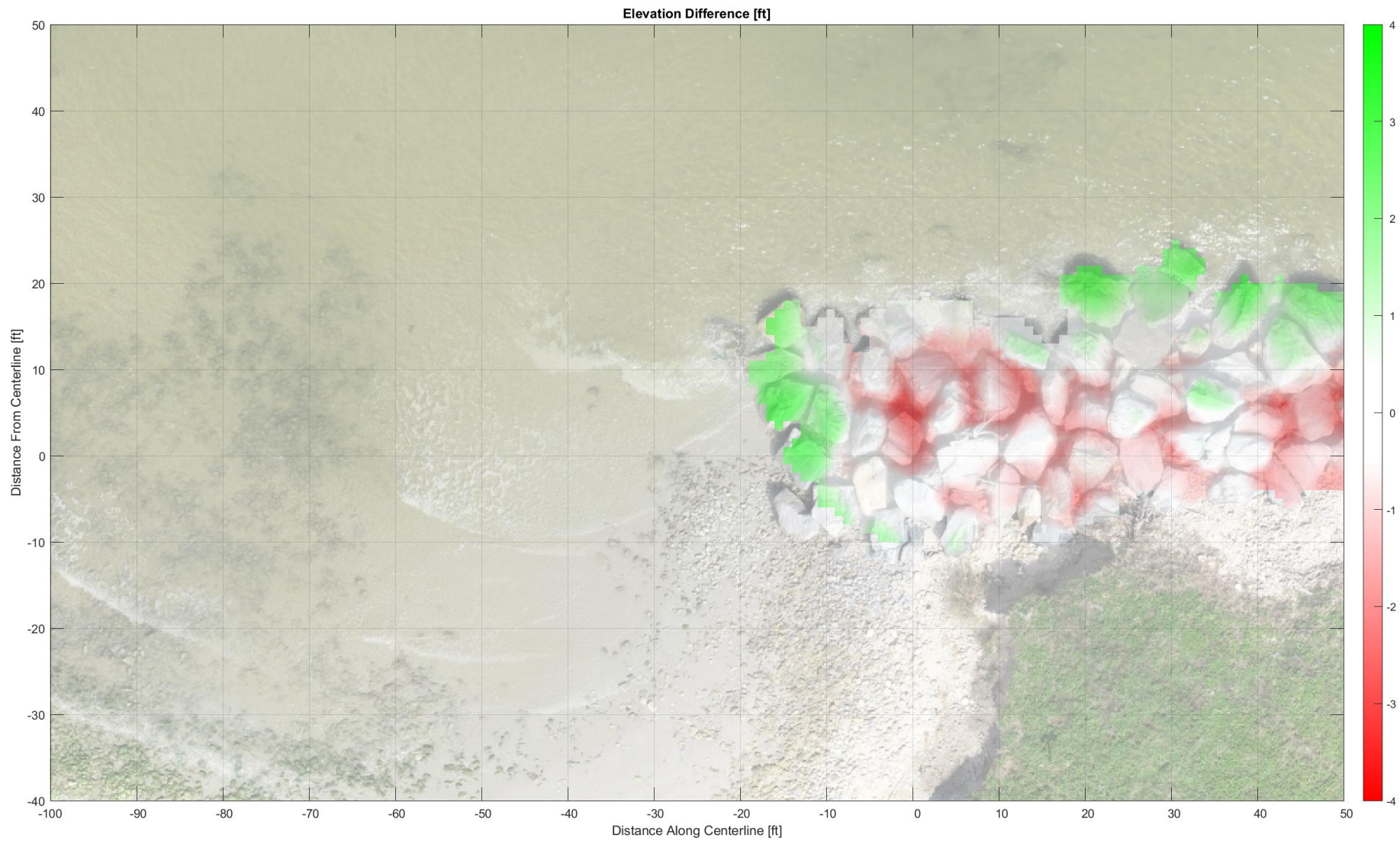
Face	Min	Max	Avg
North	1.8	4.8	3.1
South	0.5	6.1	2.9

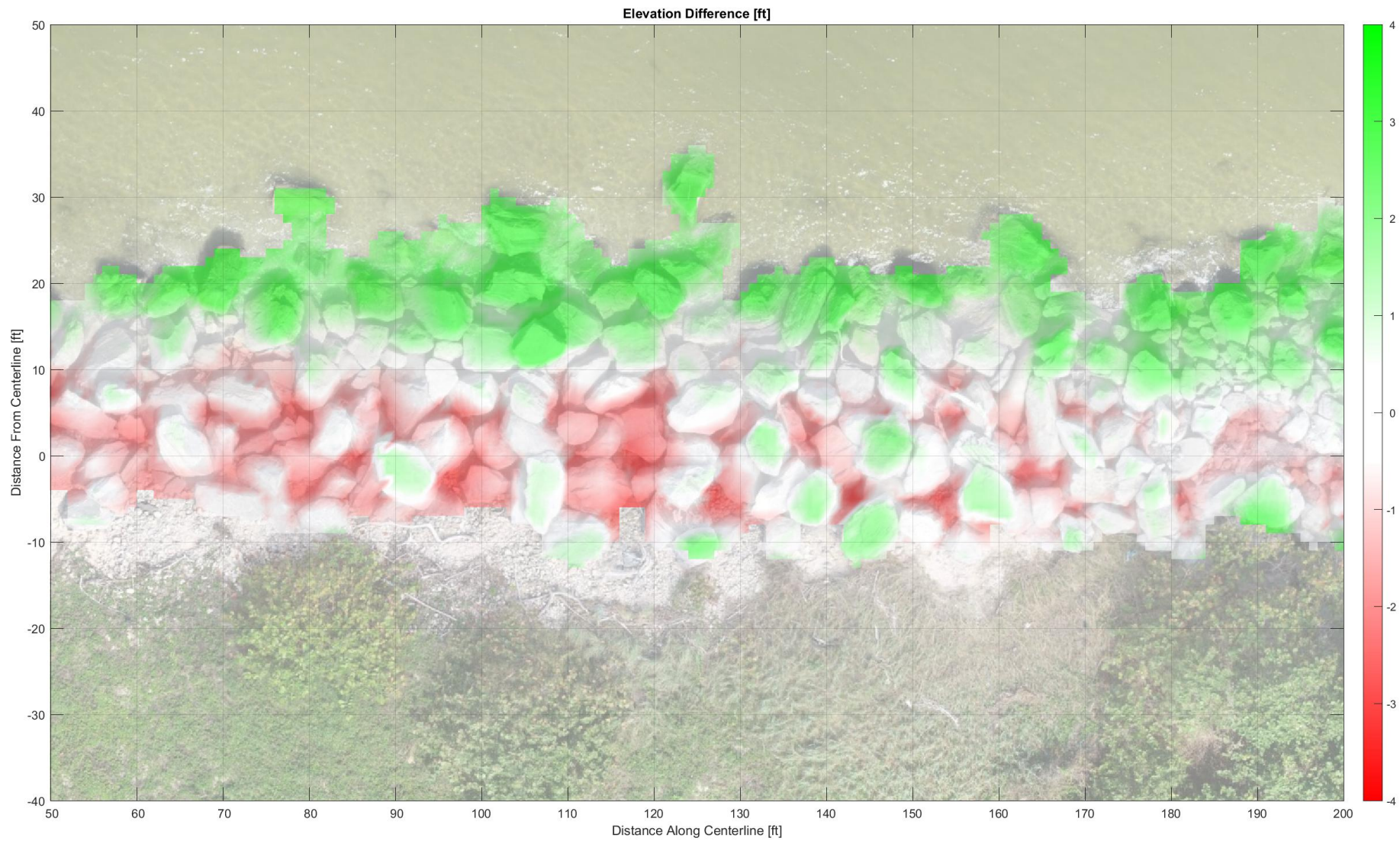
- Minimum, maximum, and average stone sizes were calculated for each 20-foot segment along the north and south jetty faces.

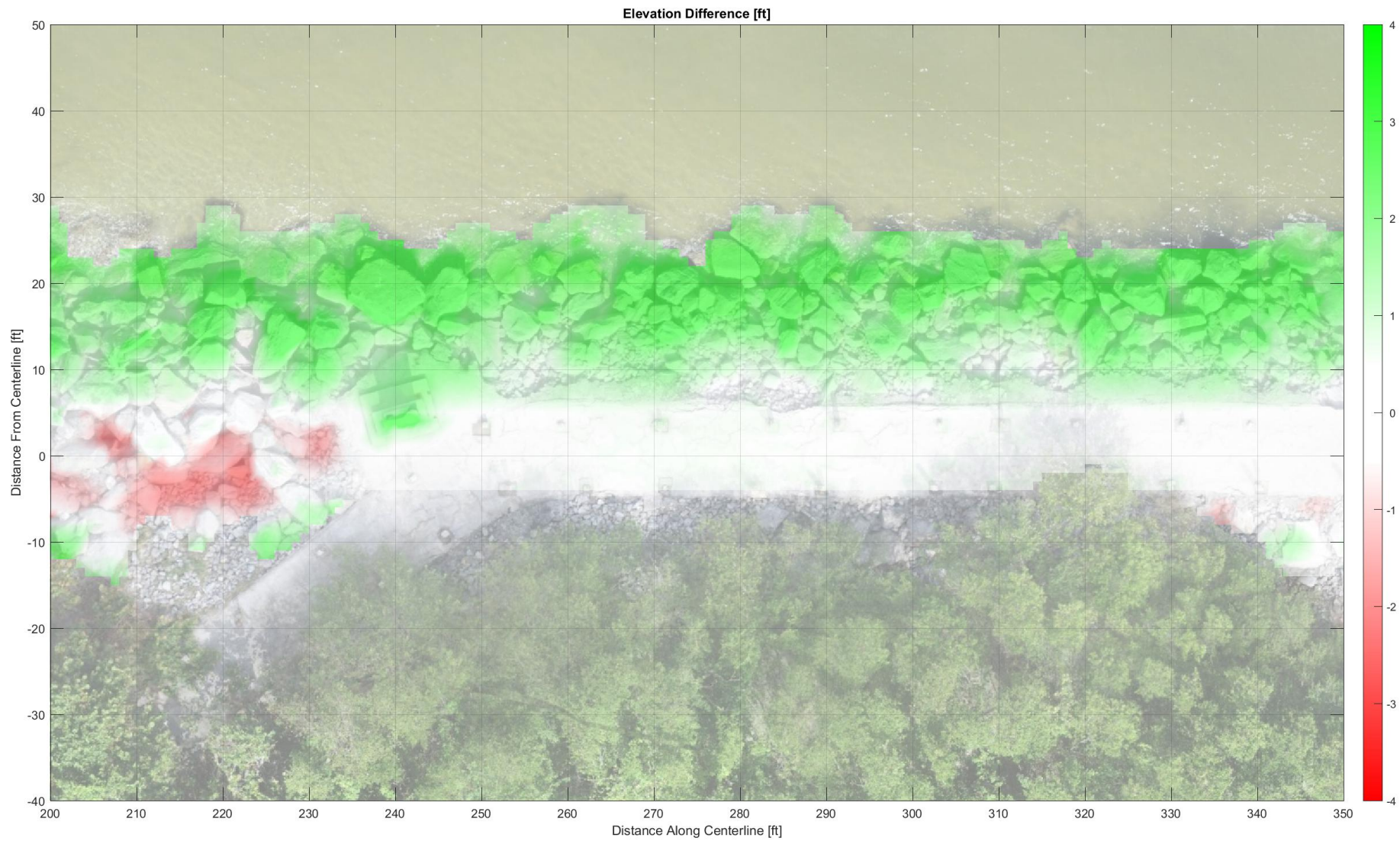


Elevation Difference [ft]

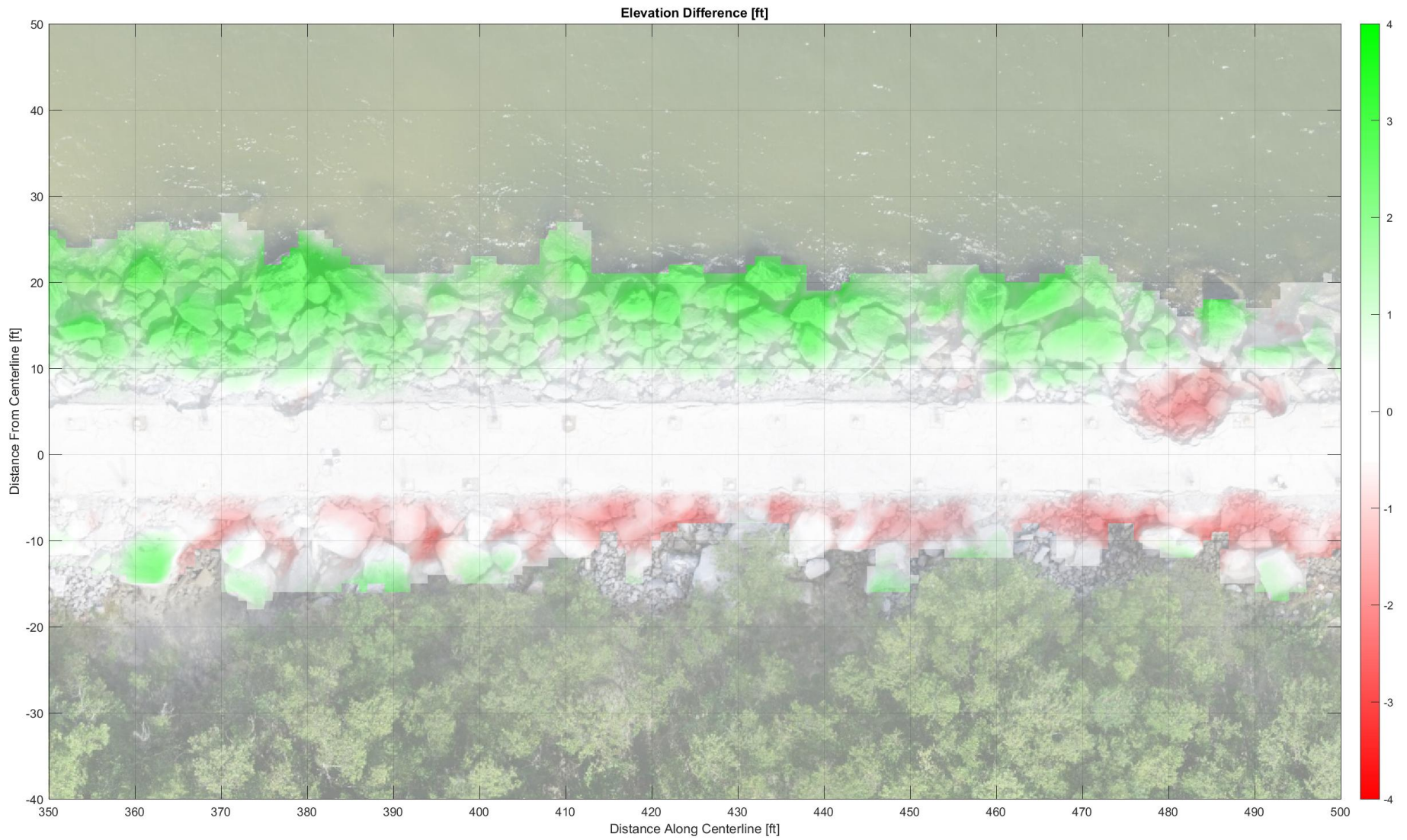


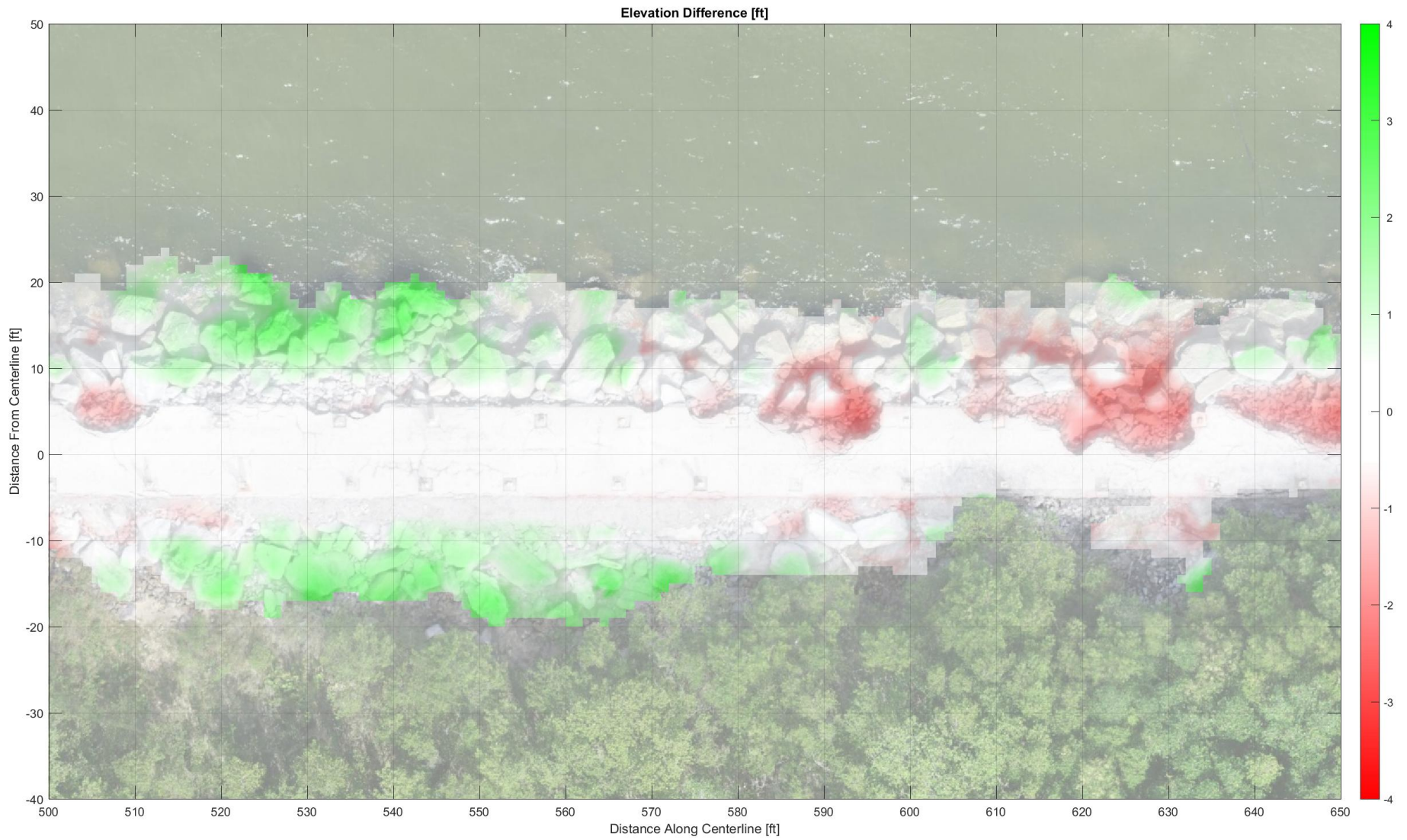


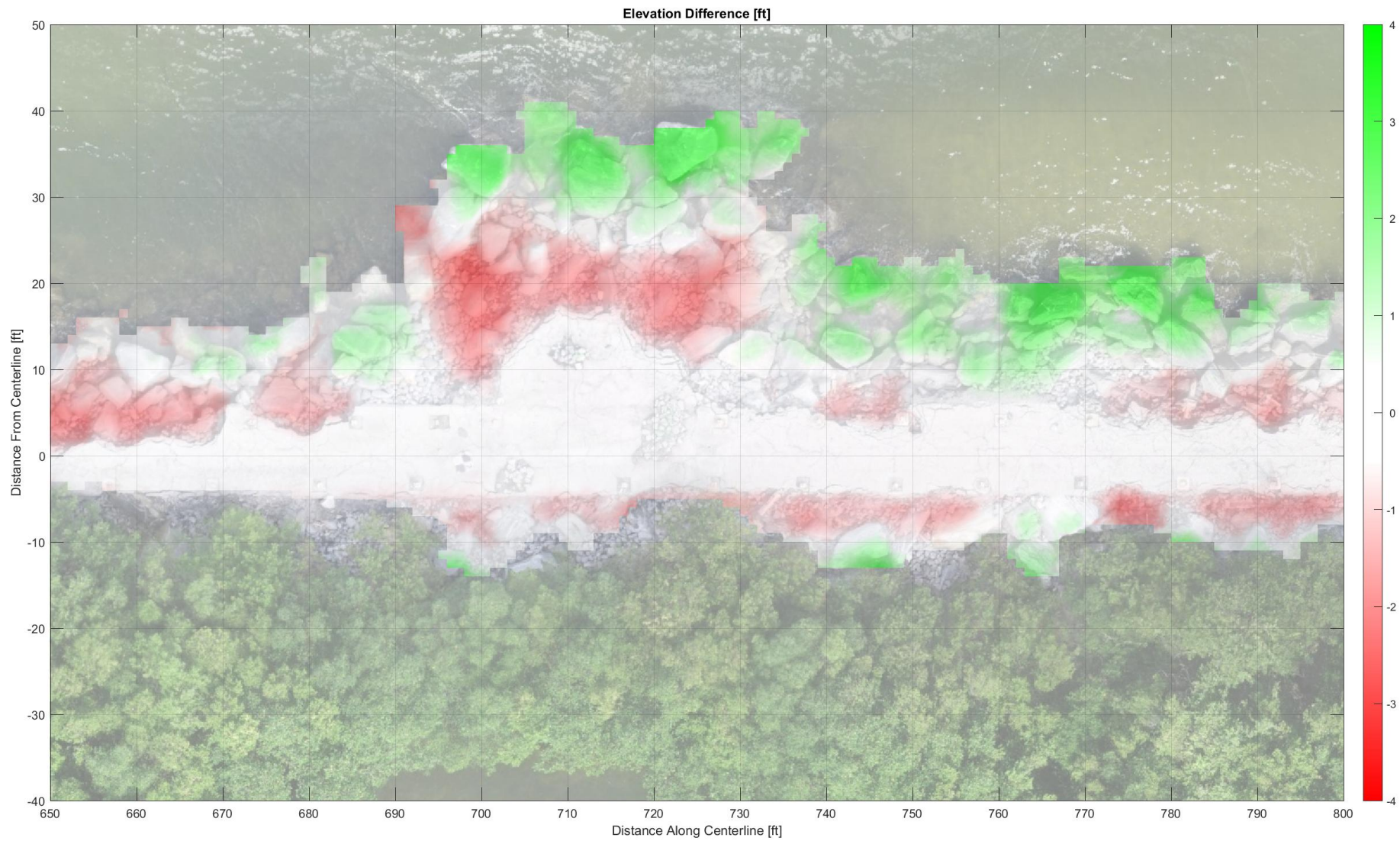


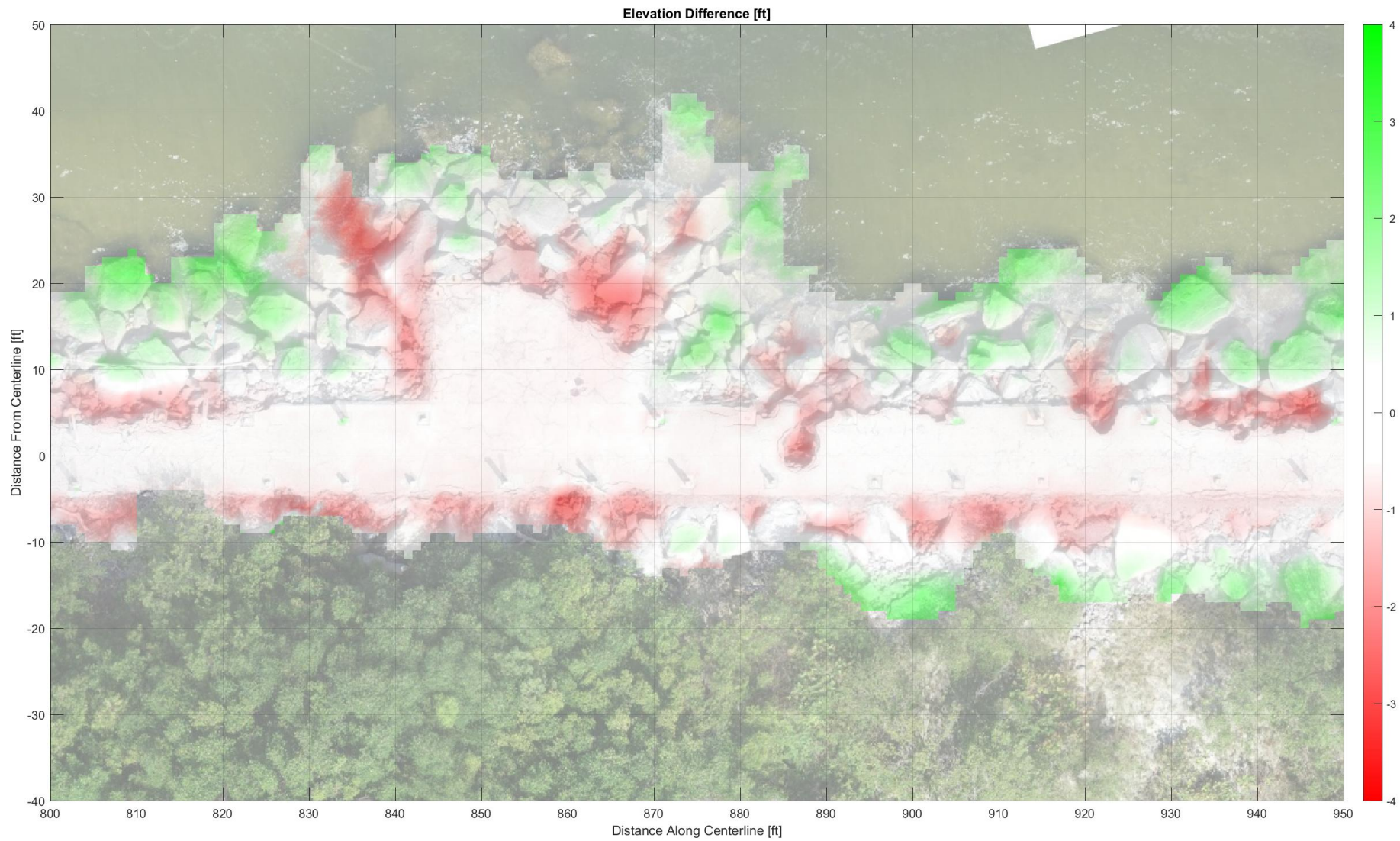


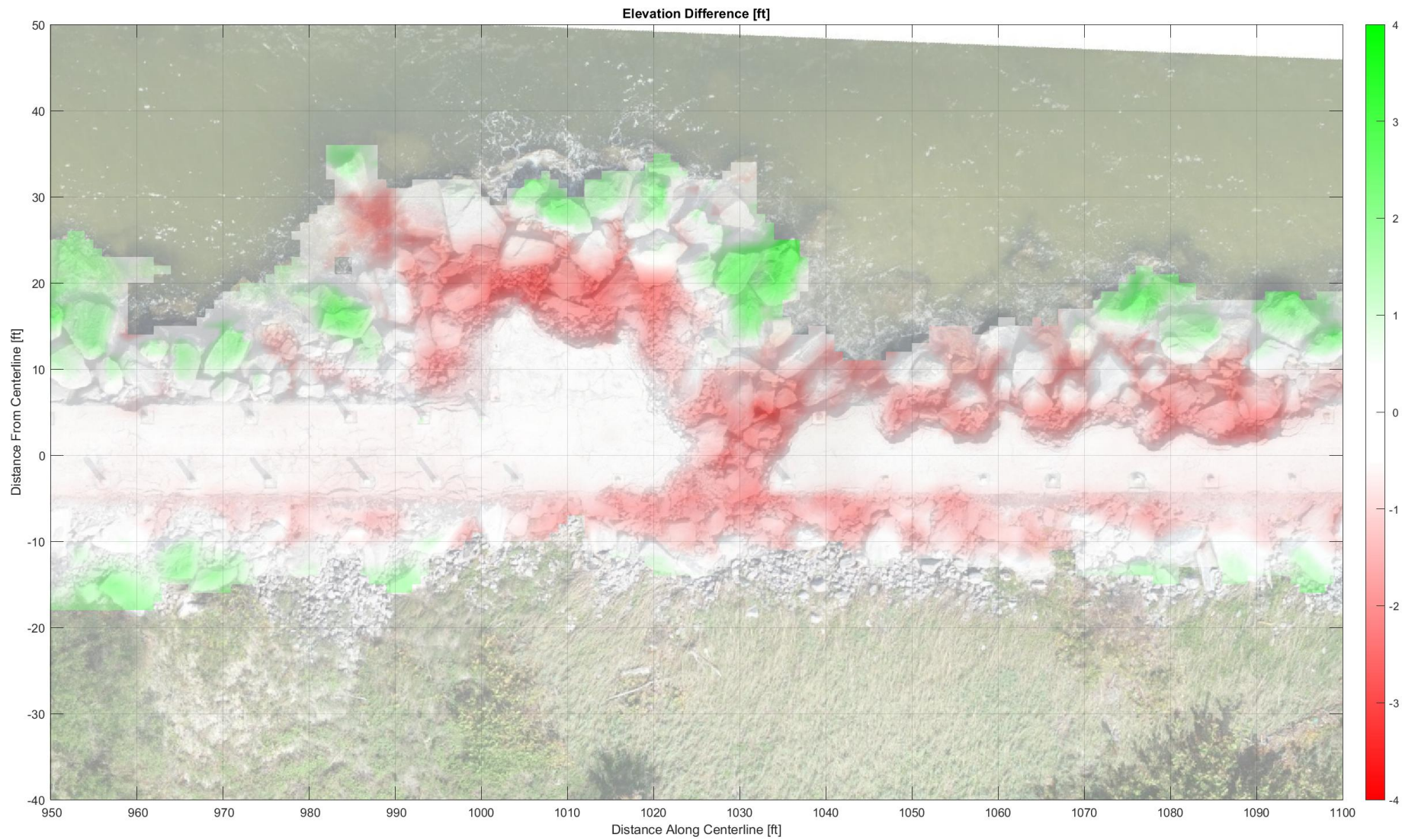


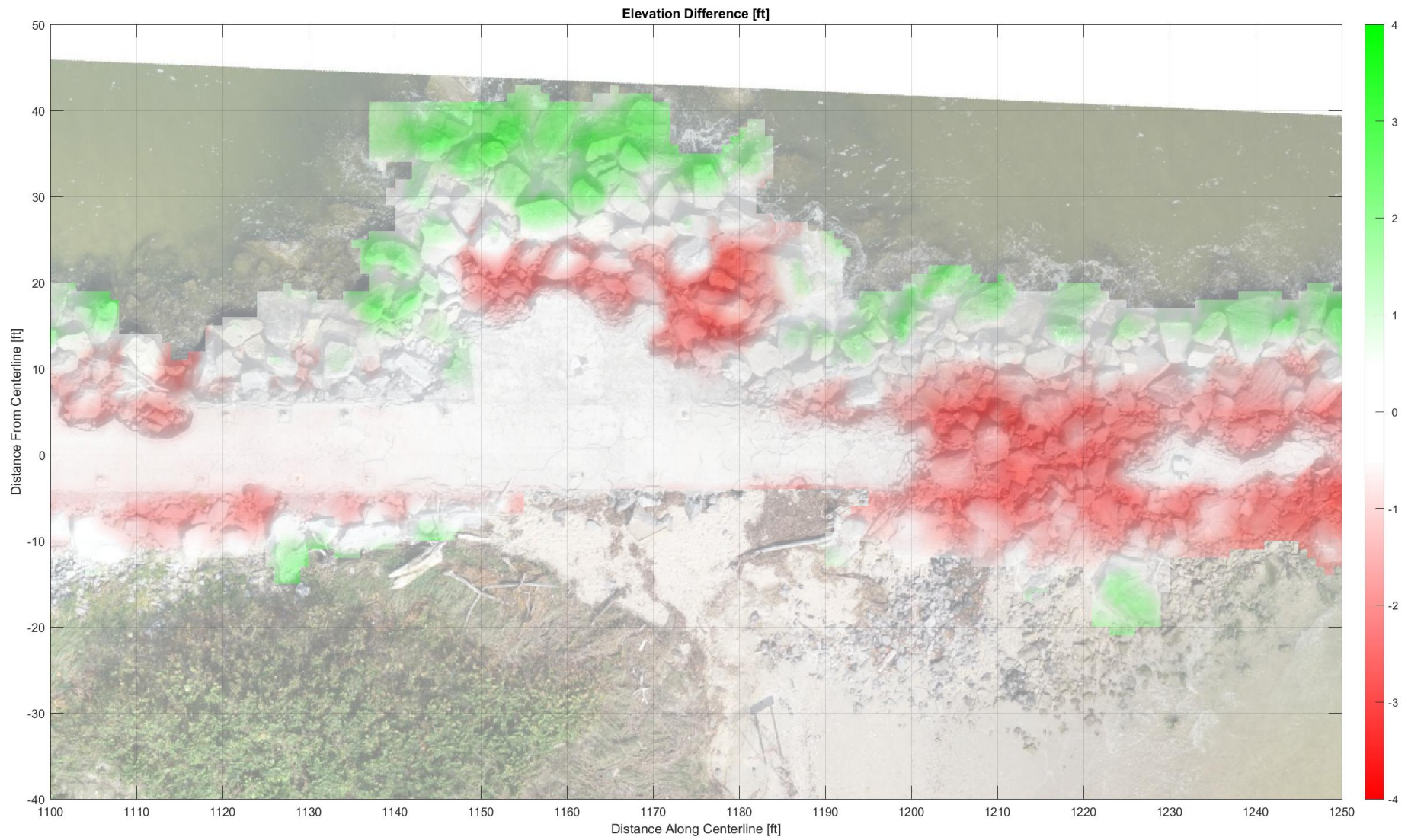


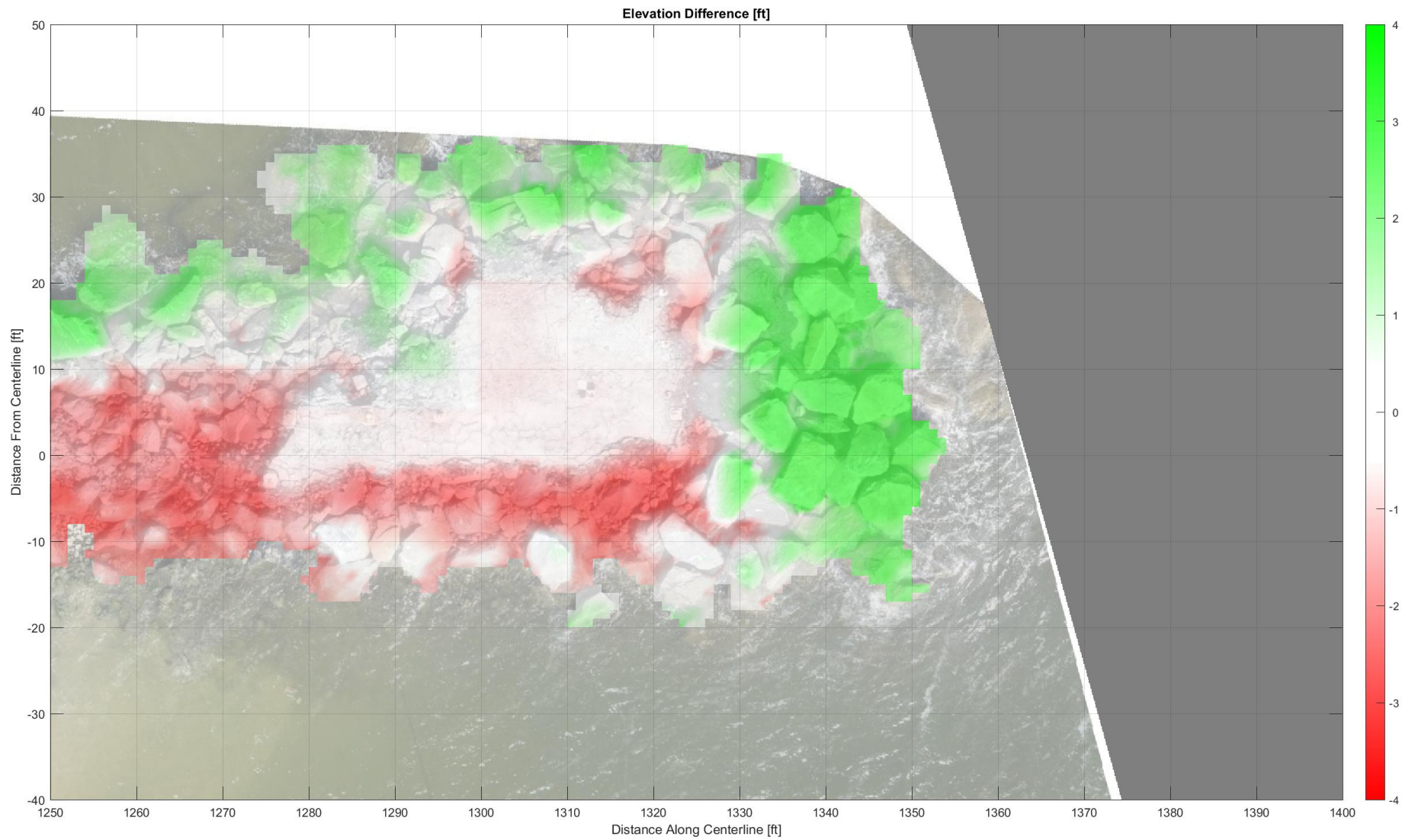




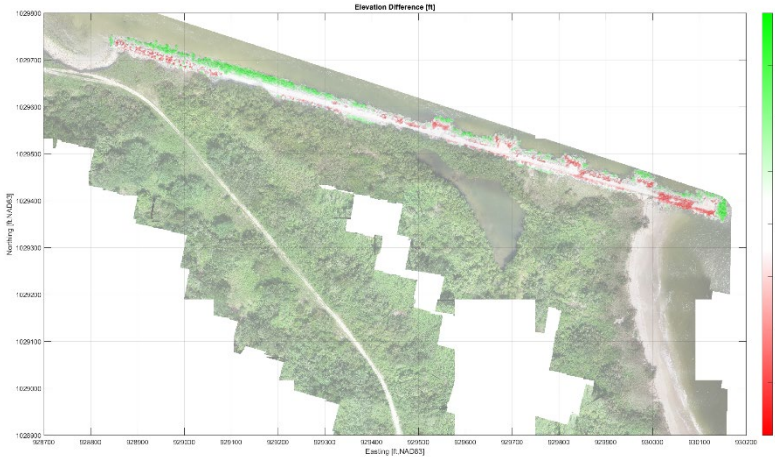








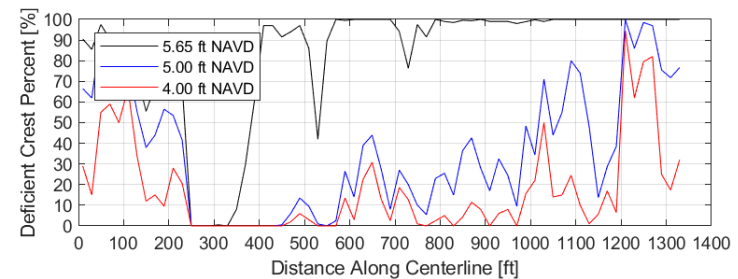
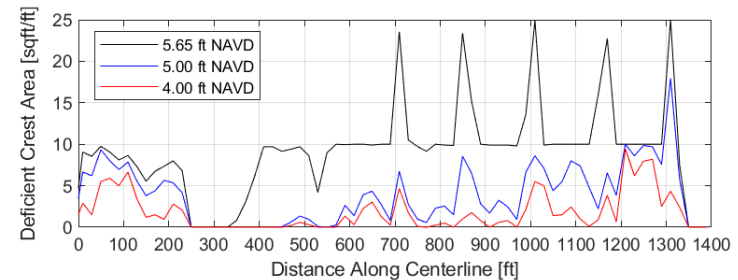
# JETTY ELEVATION COMPARISONS



- › Elevation deficiencies were calculated for each 20-foot segment along the jetty crest.

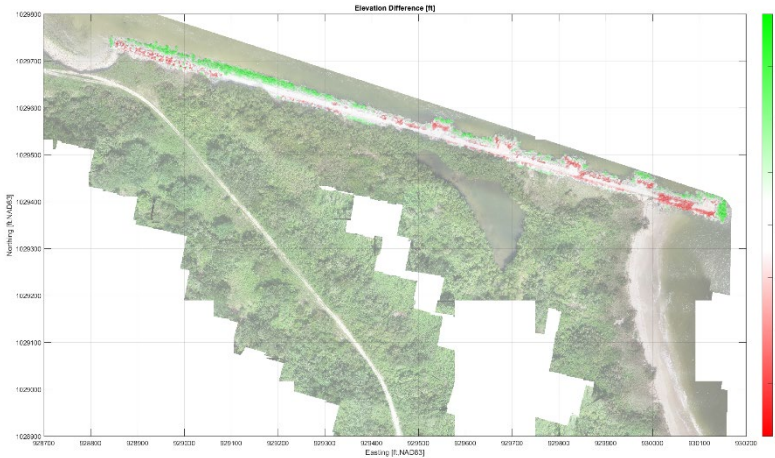
## › Crest Elevation Deficiency (sqft)

Quantity	< 5.65	< 5.00	< 4.00
Area	12,890	5,420	2,530
Percent	85%	6.1%	2.9%





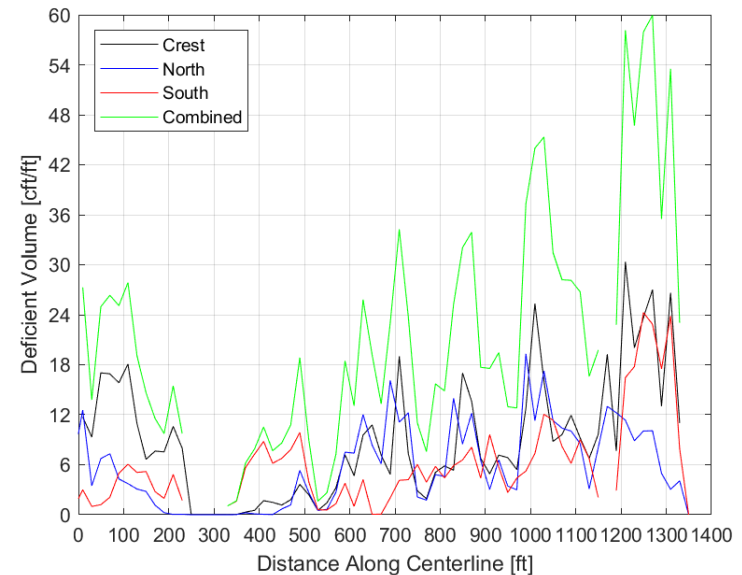
# JETTY VOLUME COMPARISONS



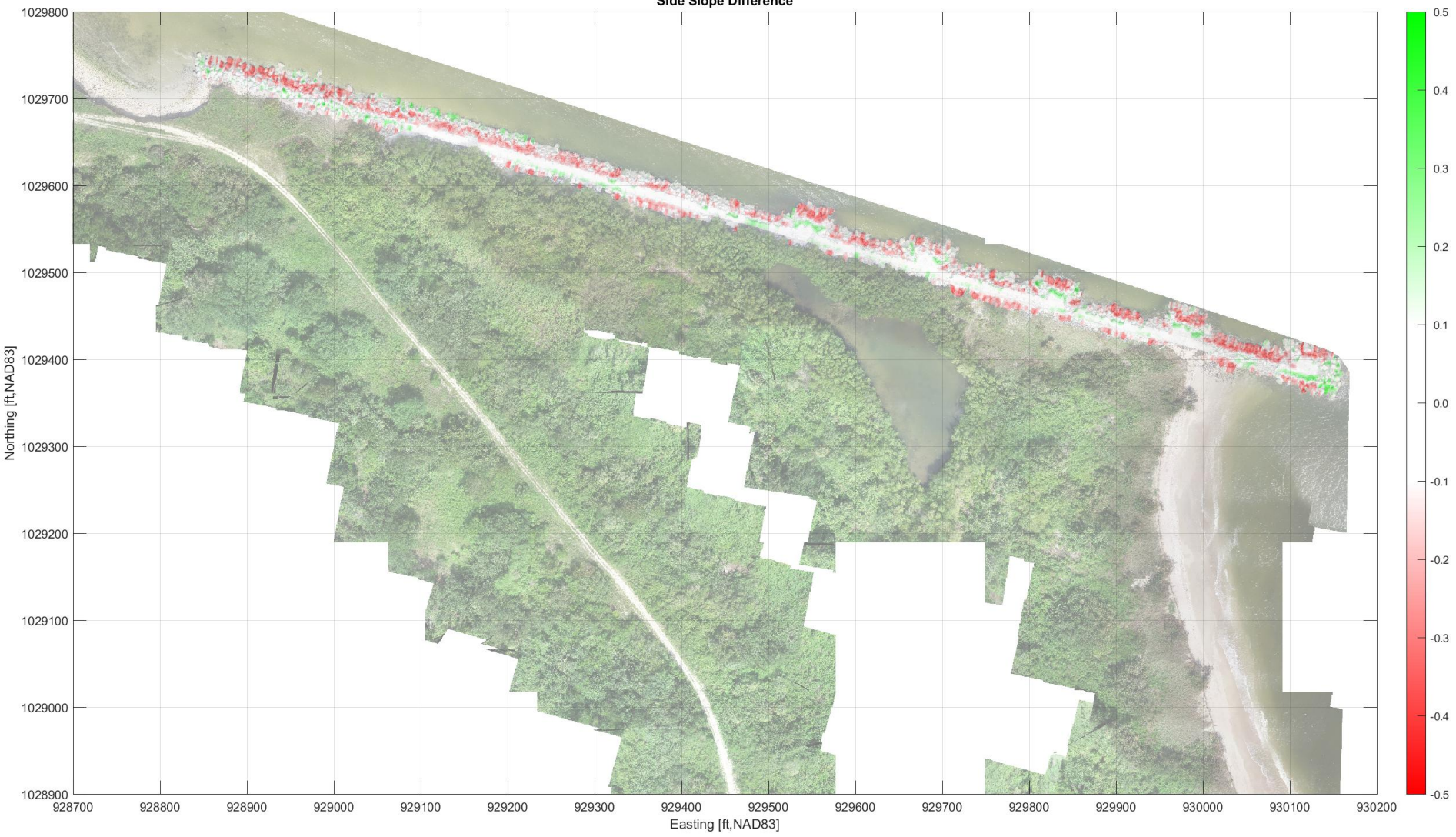
› Volumetric requirements were calculated for each 20-foot segment along the jetty.

## › Stone Placement Requirements

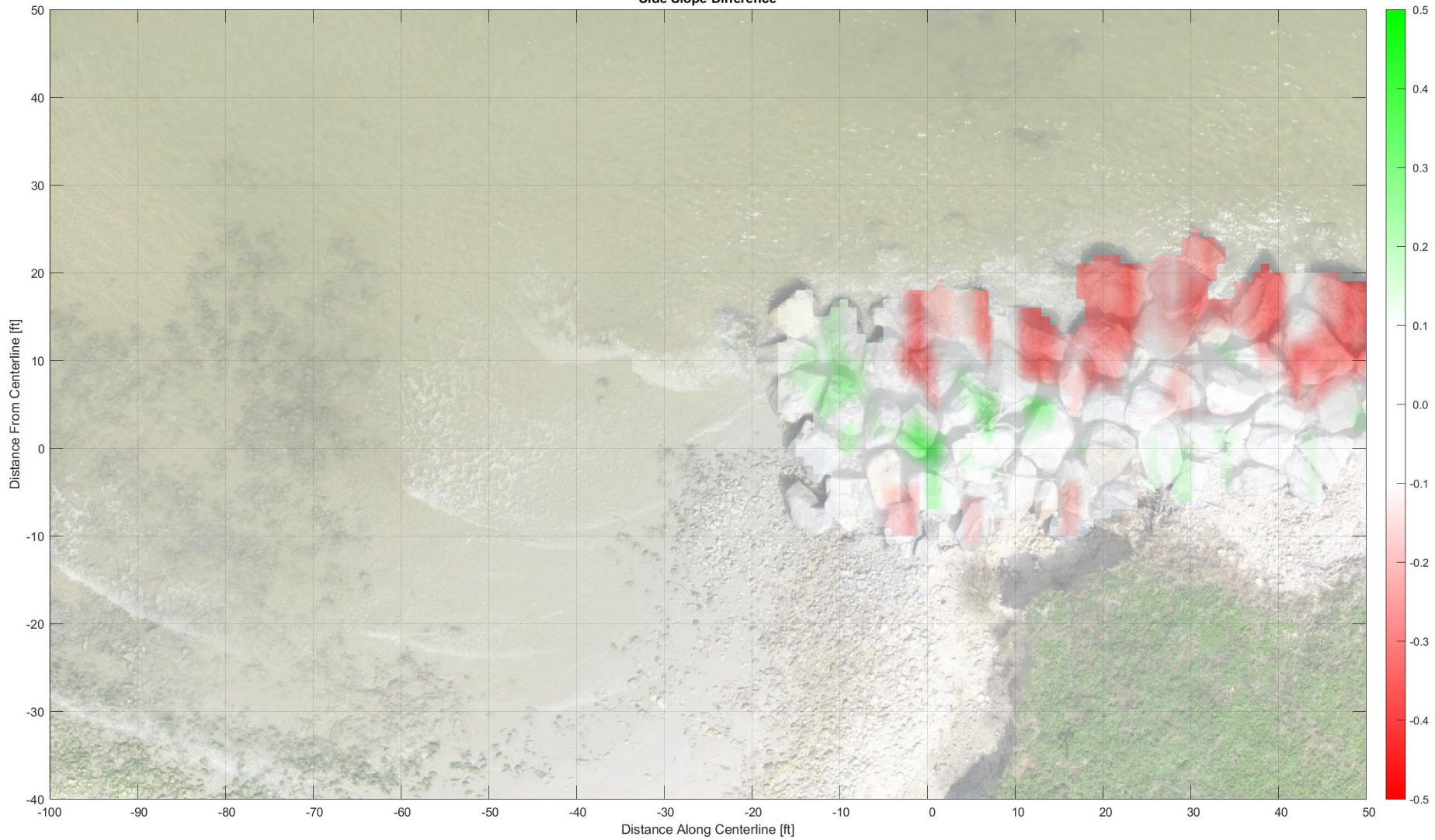
Face	Volume (cft)	Weight (tons)
Crest	12,450	1,030
North	7,940	650
South	8,480	700
<b>Total</b>	<b>28,870</b>	<b>2,380</b>

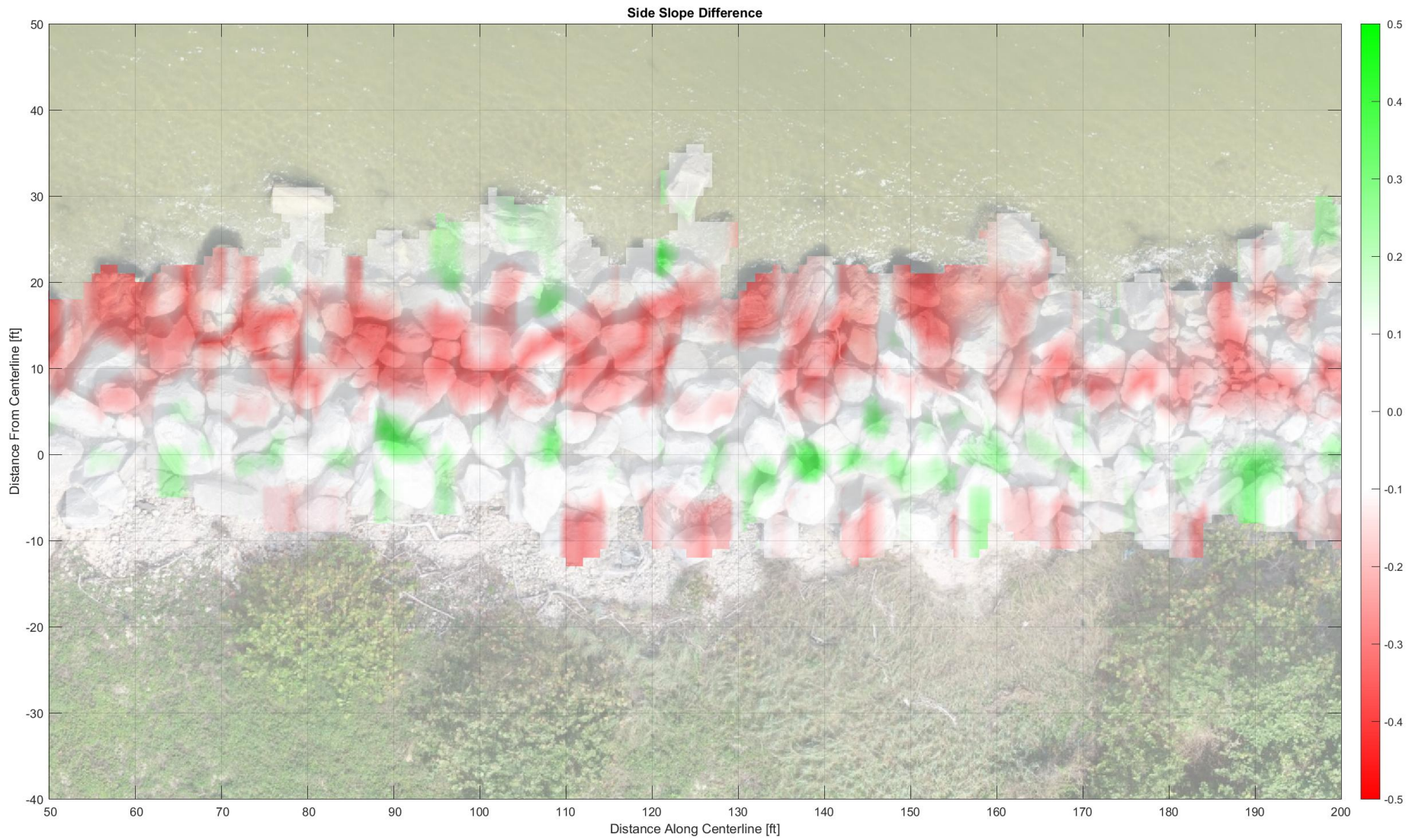


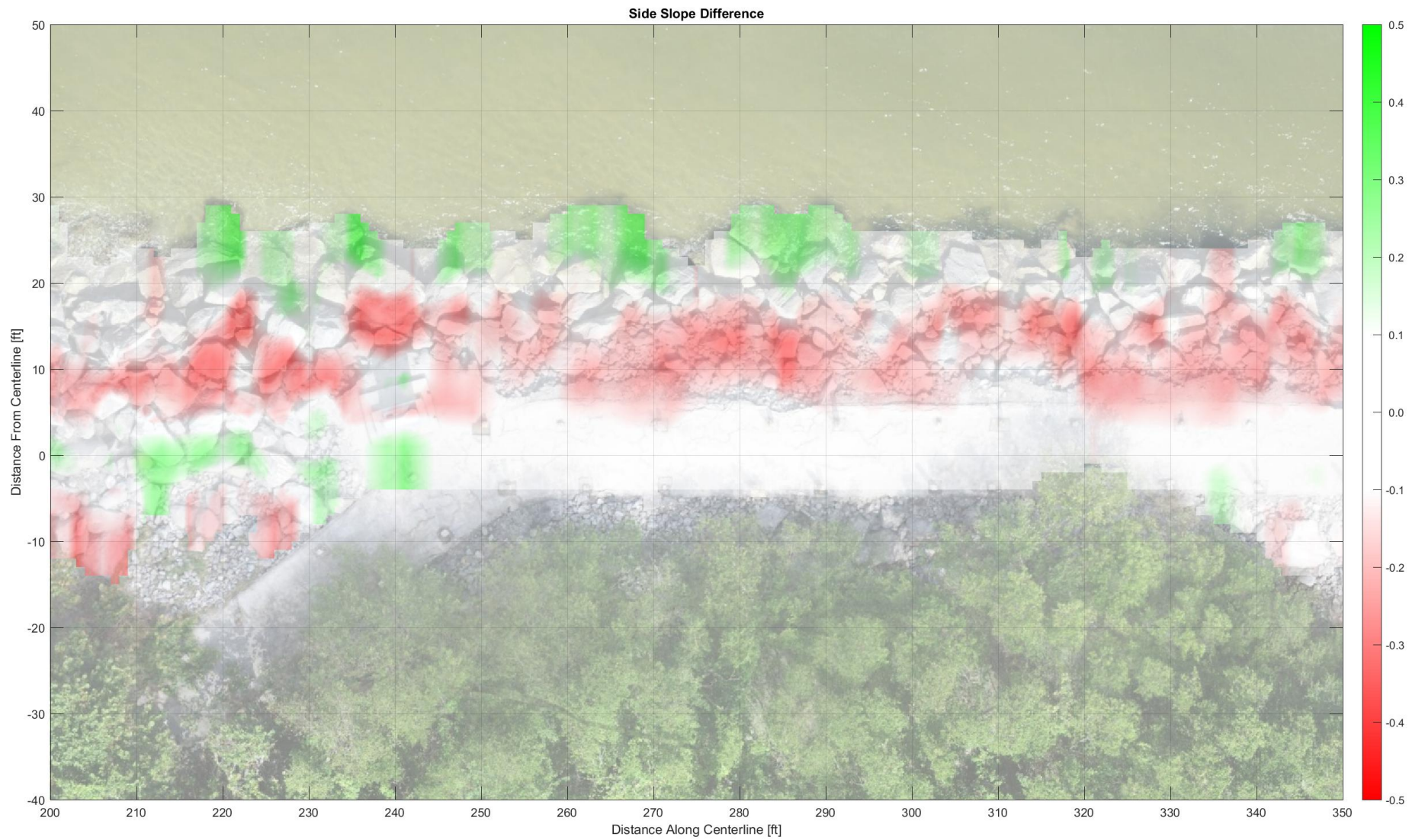
Side Slope Difference



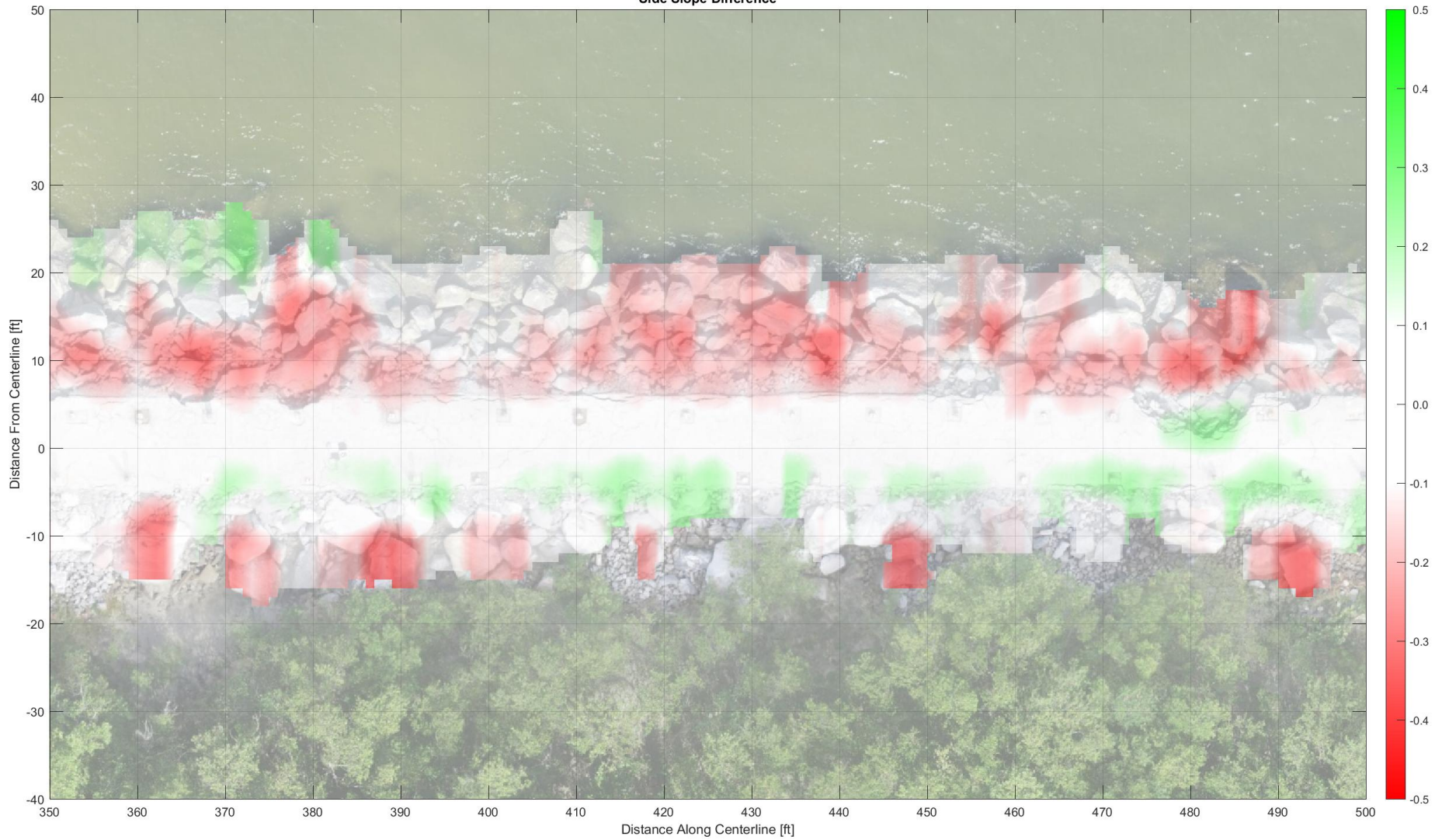
### Side Slope Difference

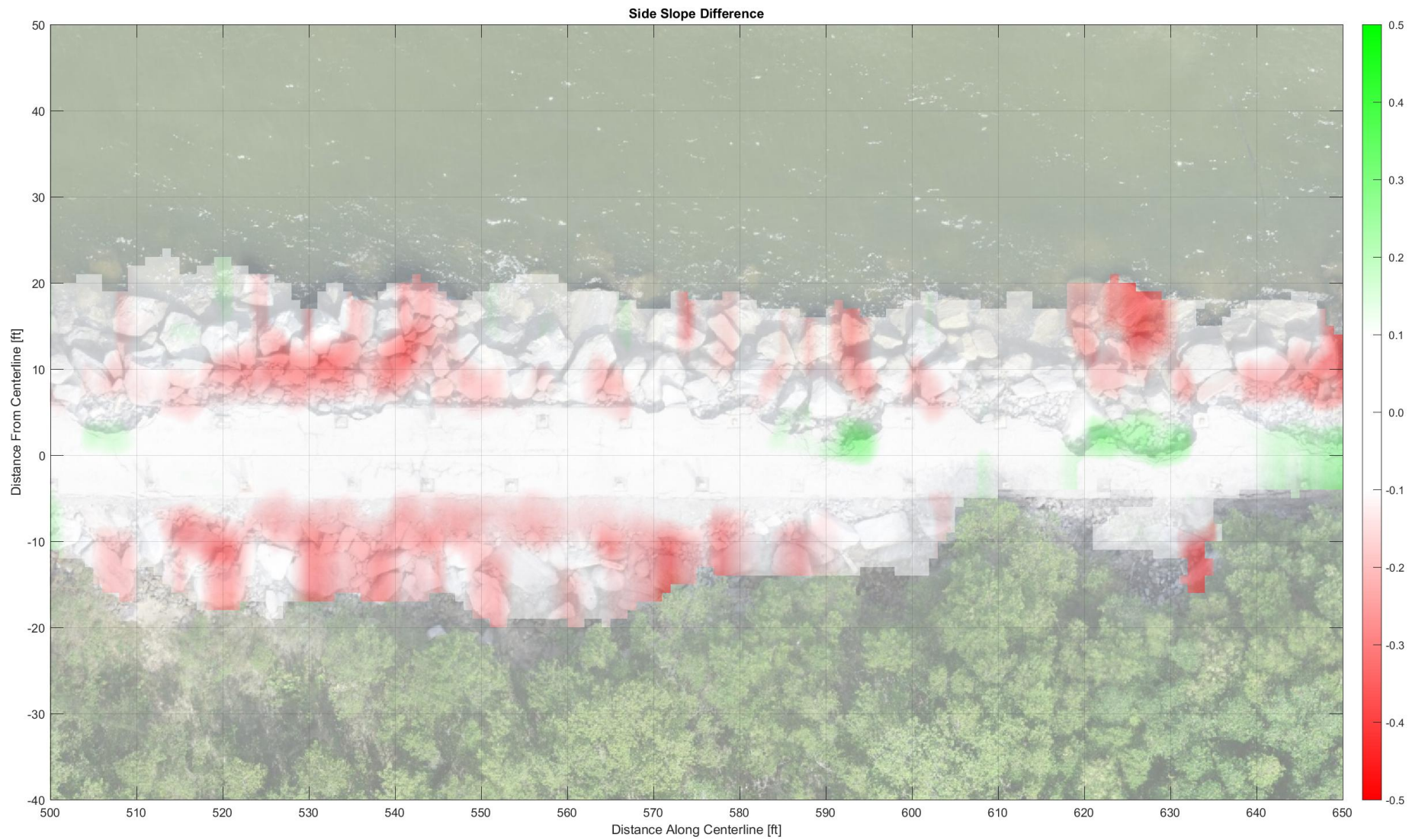


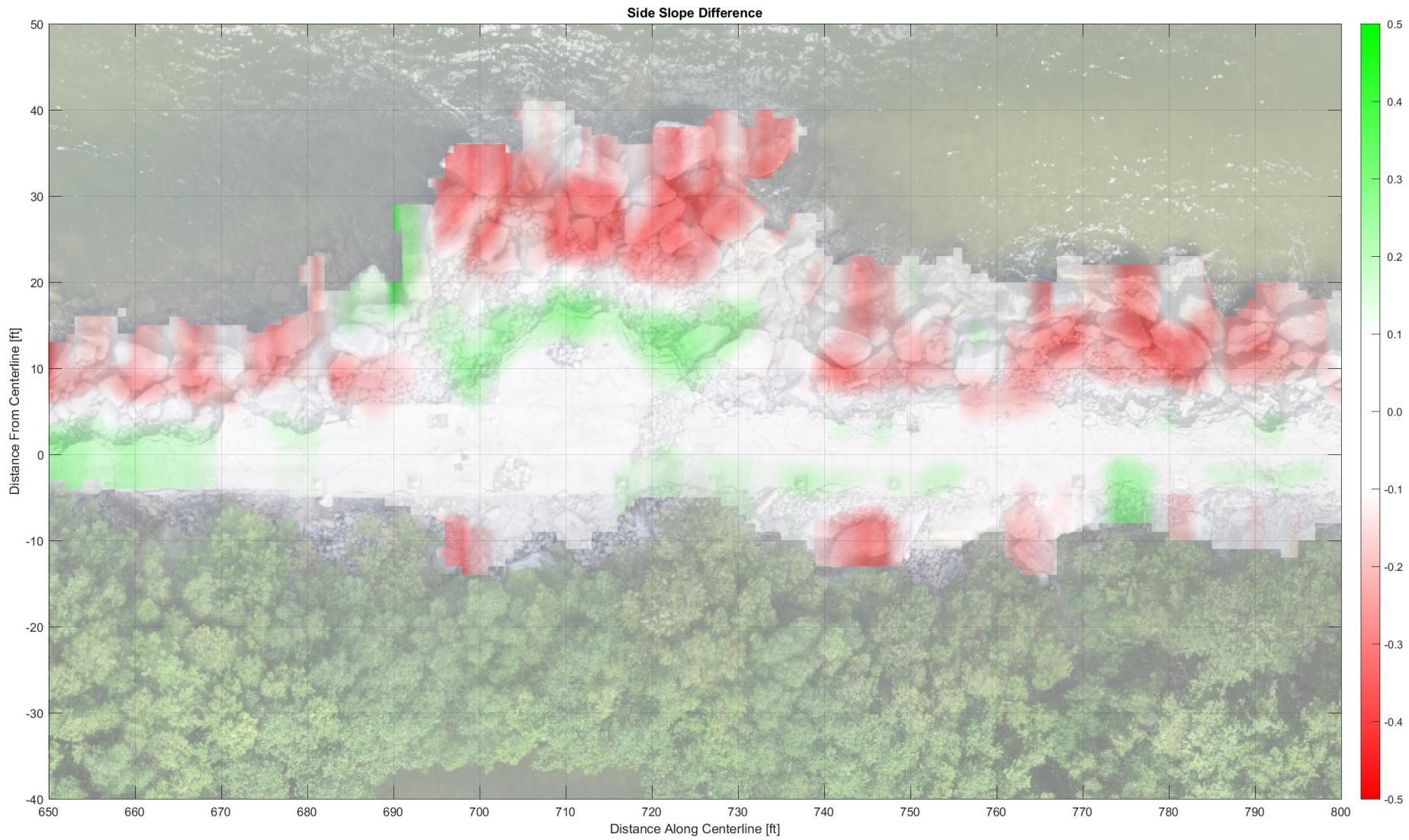




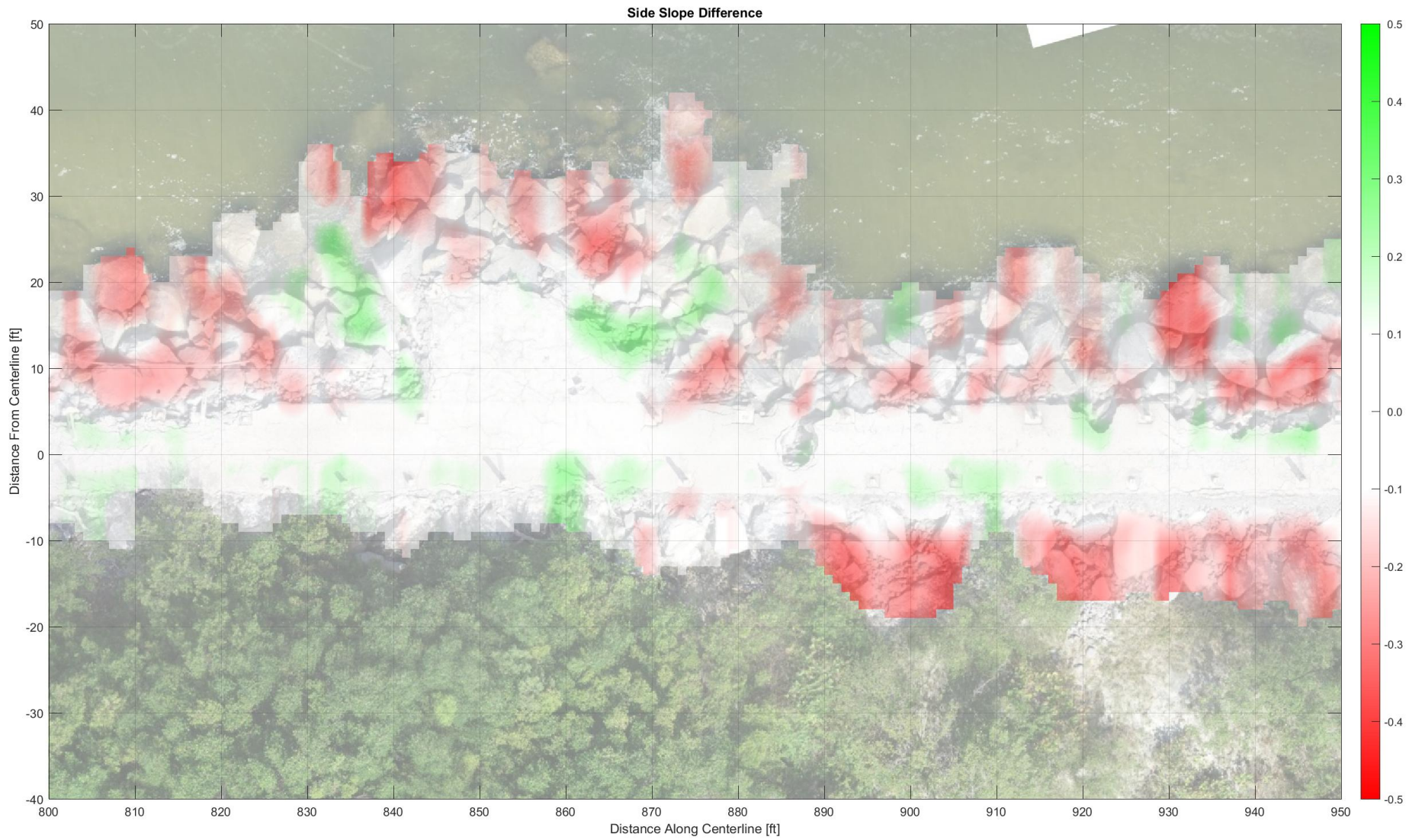
### Side Slope Difference

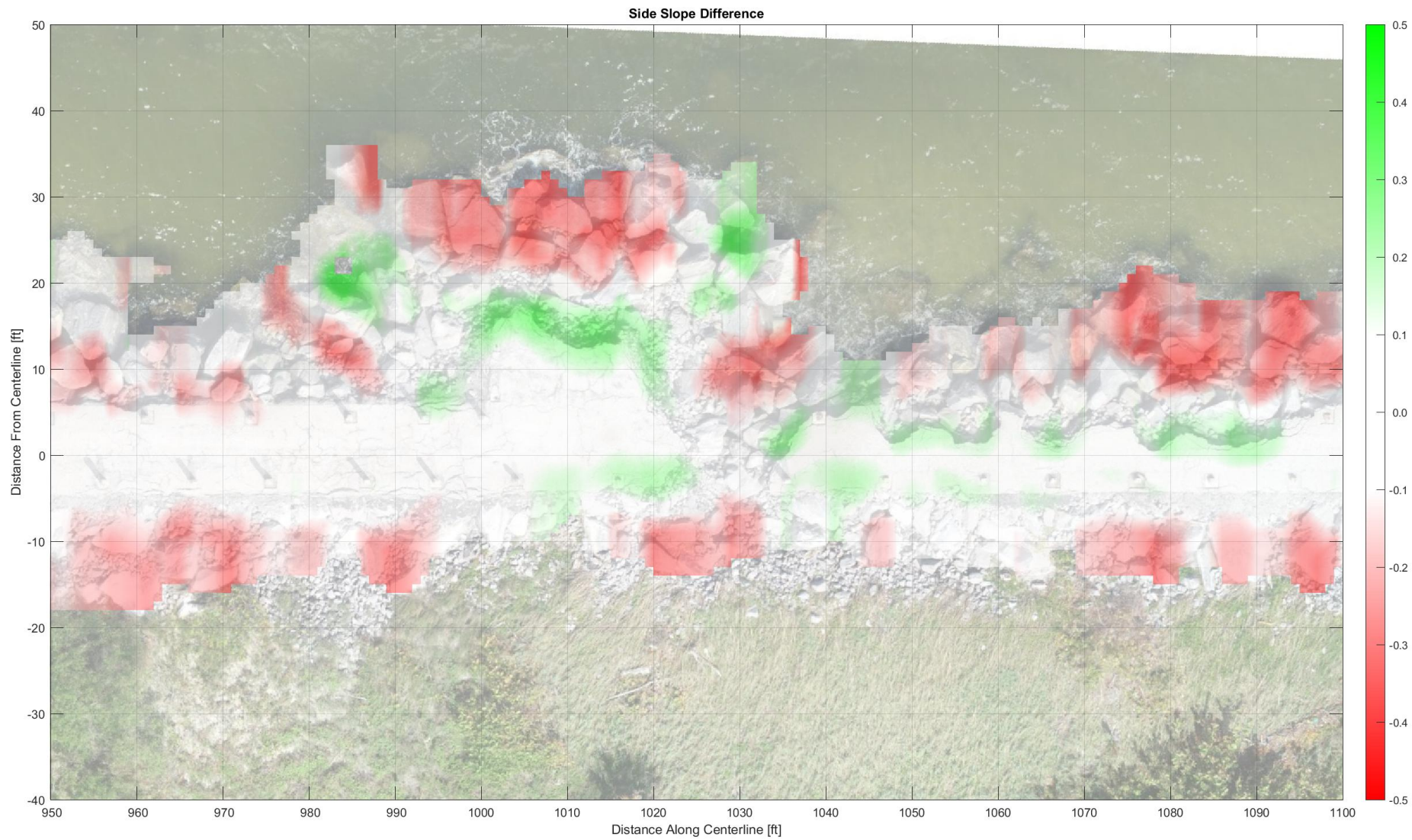


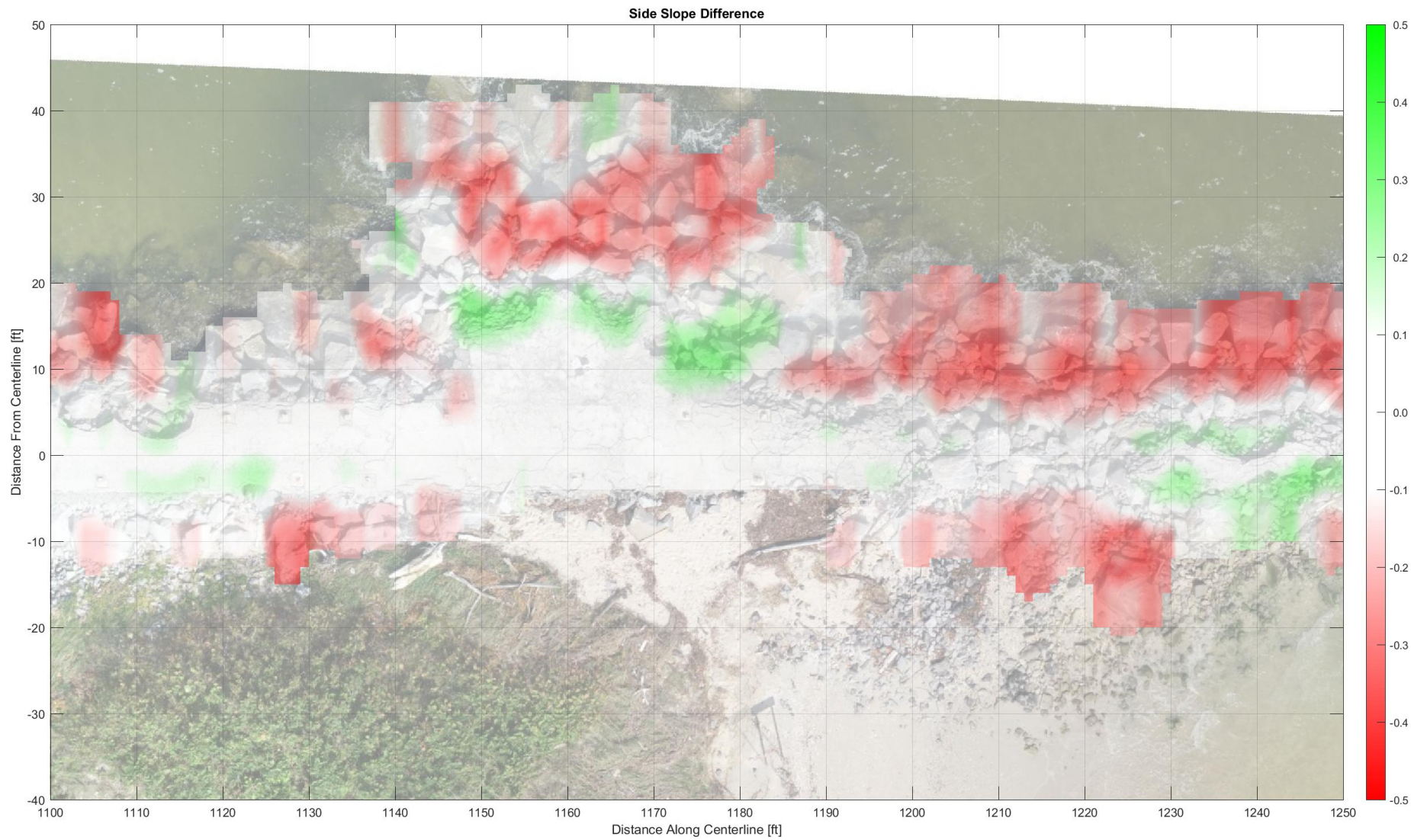


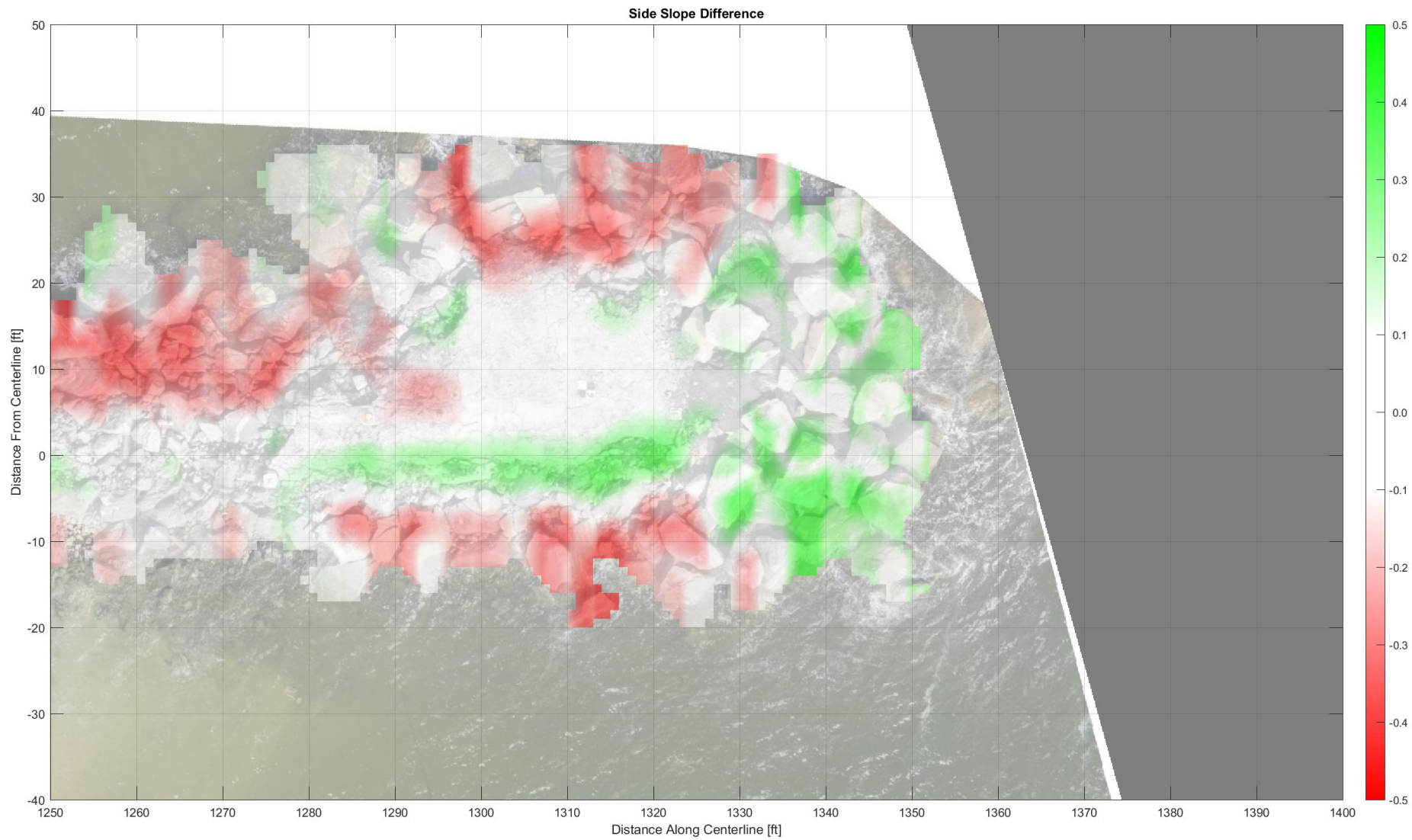




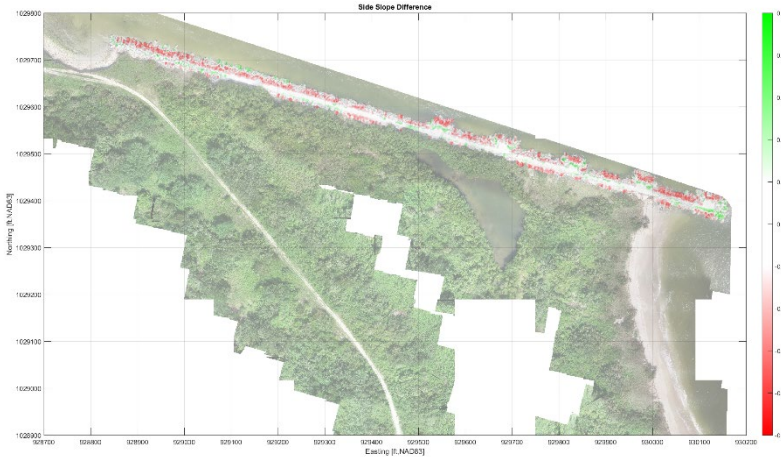








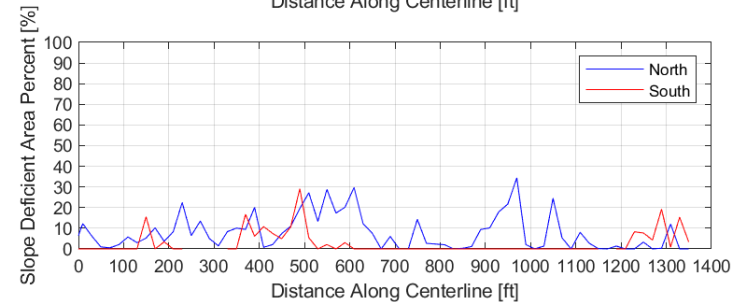
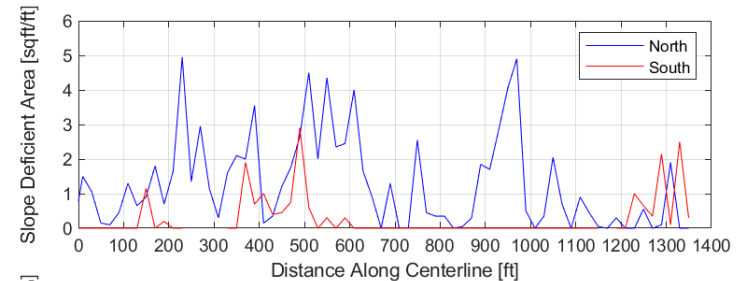
# JETTY SLOPE COMPARISONS



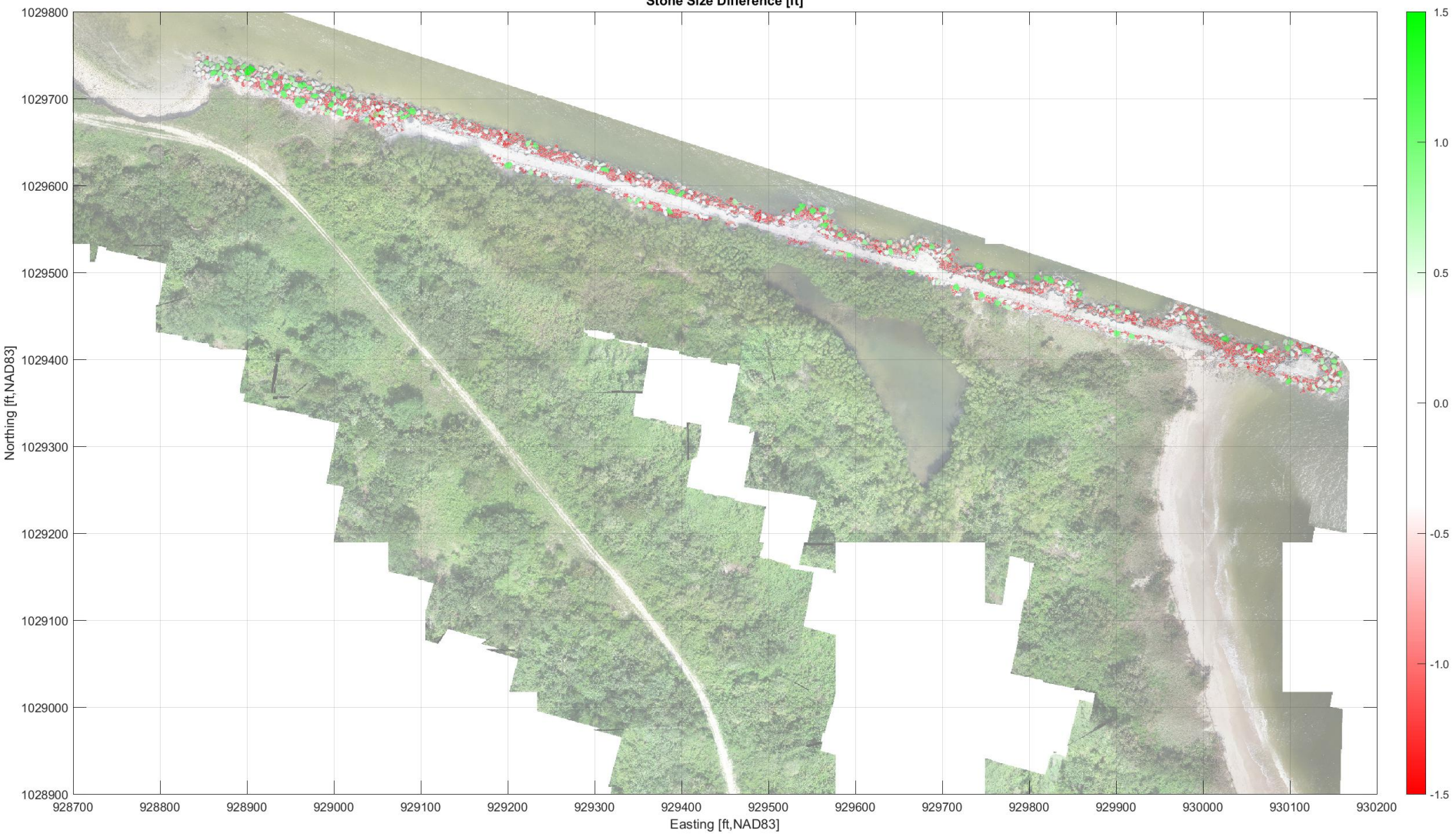
› Side slope deficiencies were calculated for each 20-foot segment along the north and south jetty faces.

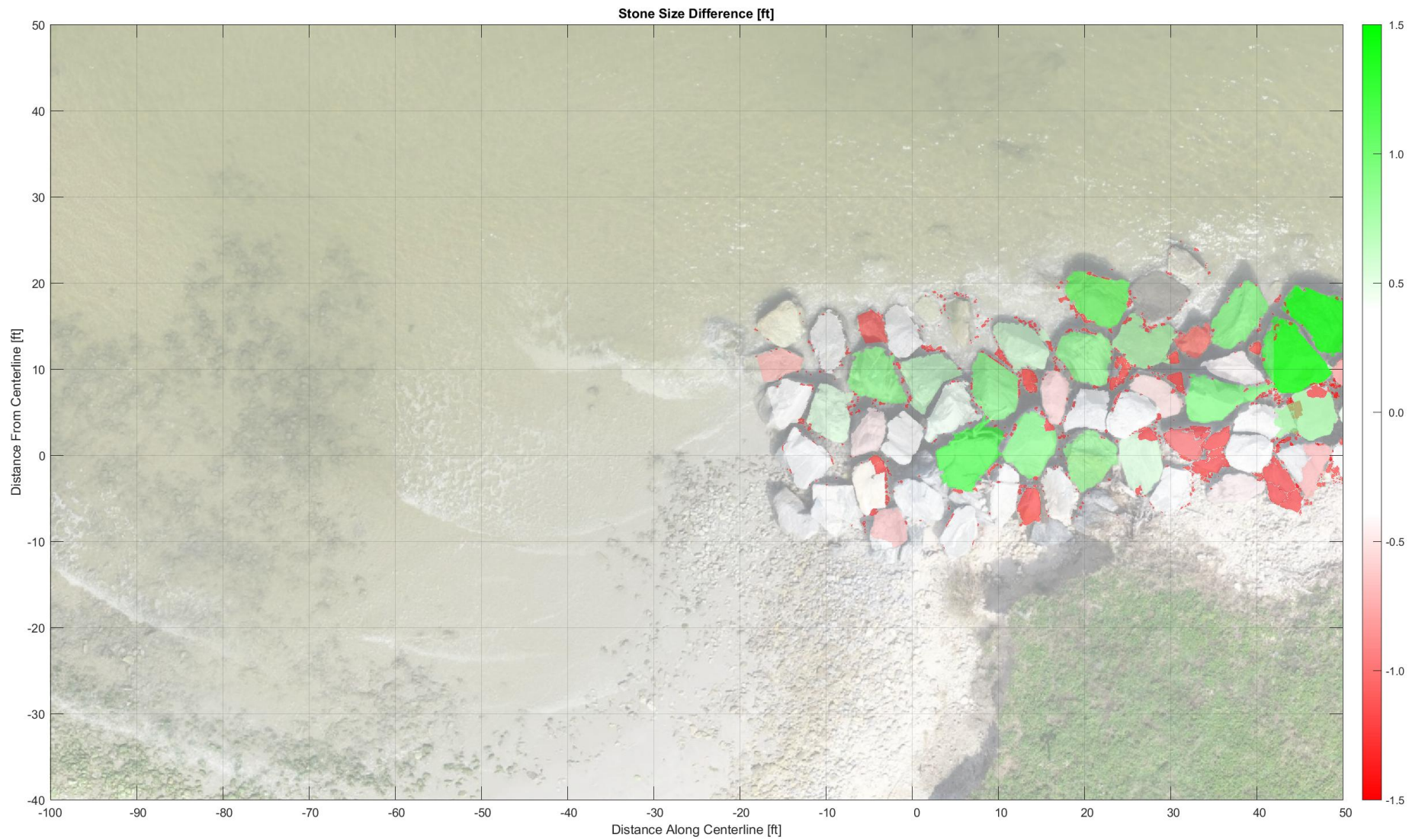
## › Side Slope Deficiency (sqft)

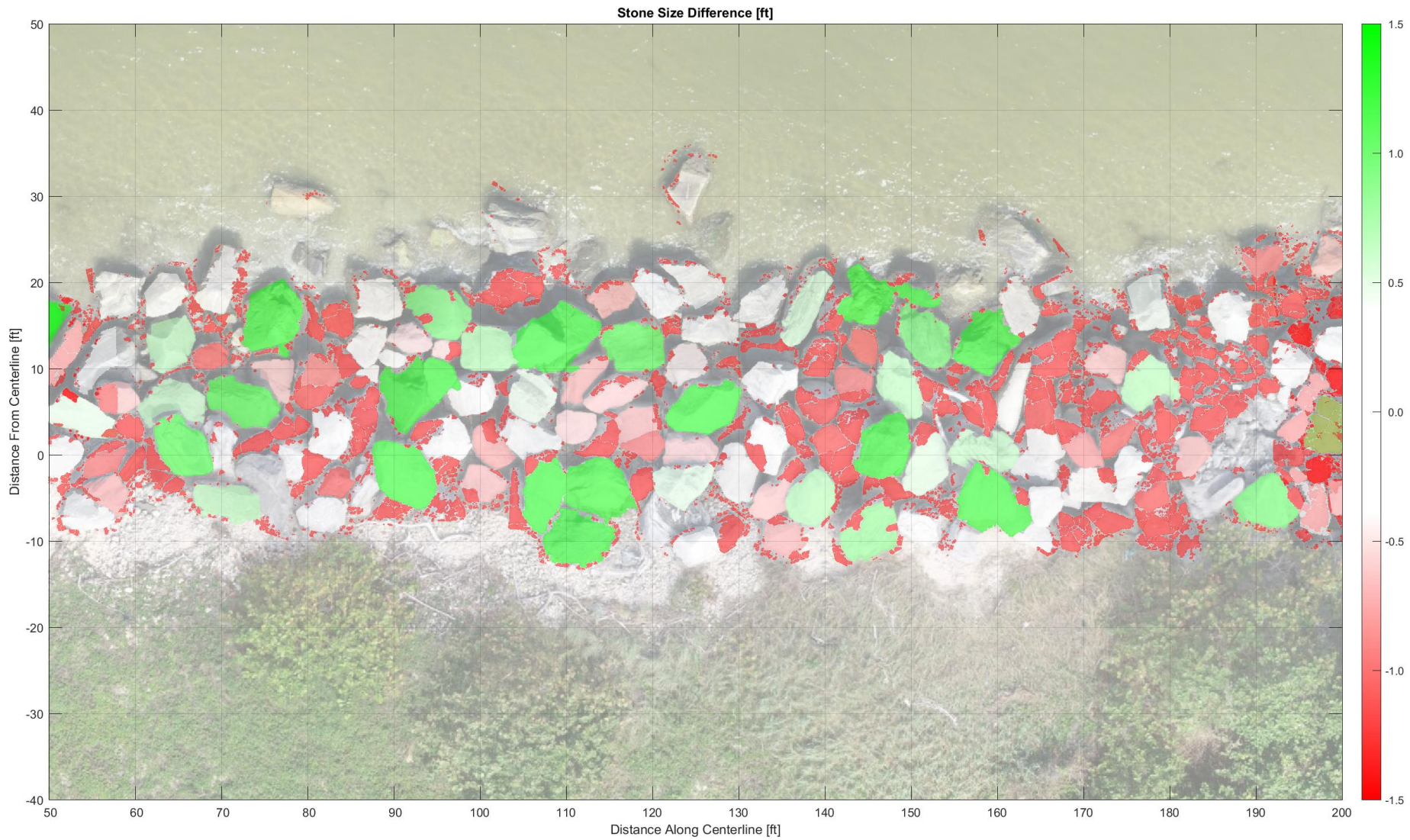
Face	Analyzed	Deficient	Percent
North	24,970	1,750	7%
South	9,780	384	4%
<b>Total</b>	<b>34,750</b>	<b>2,134</b>	<b>6%</b>



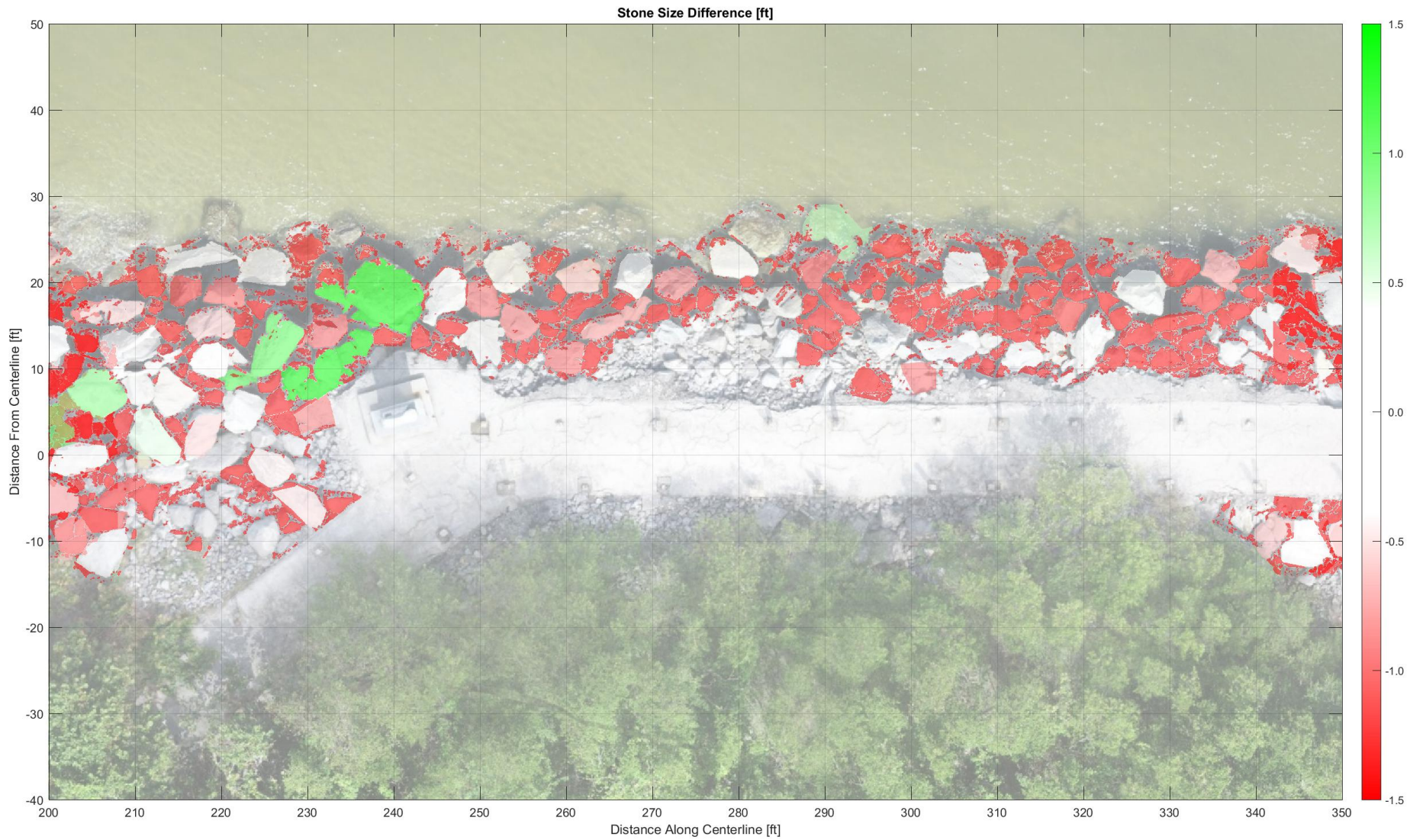
Stone Size Difference [ft]

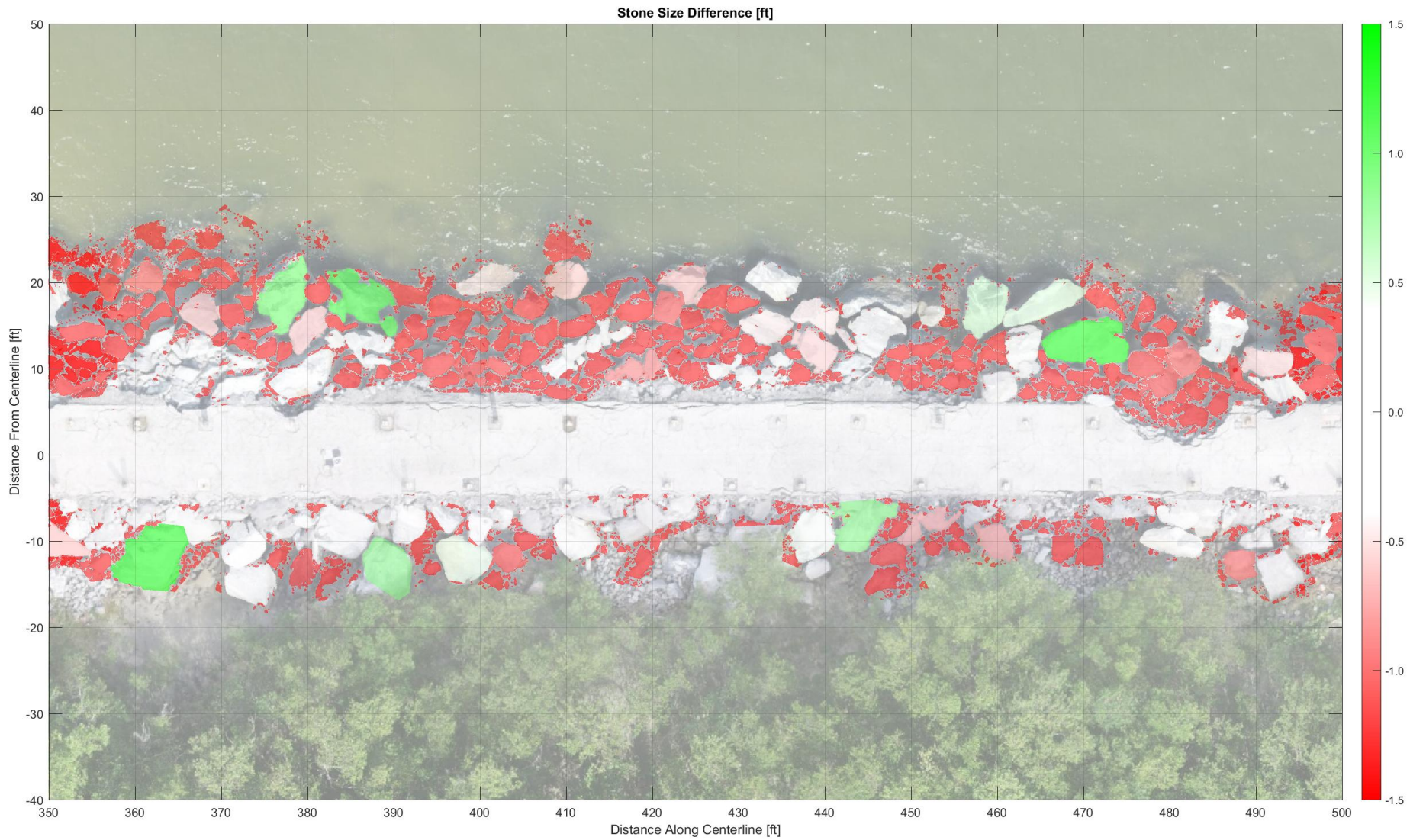


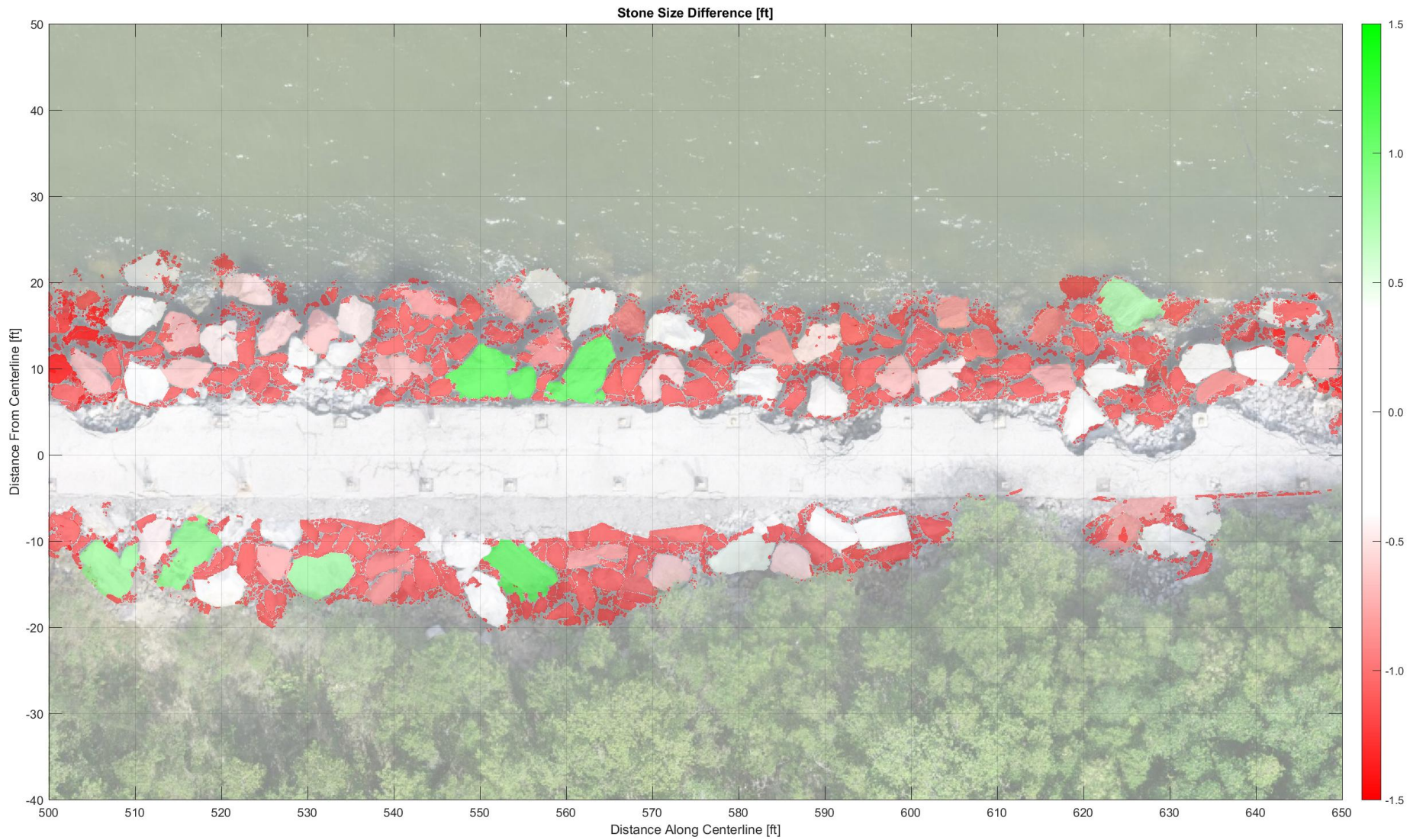


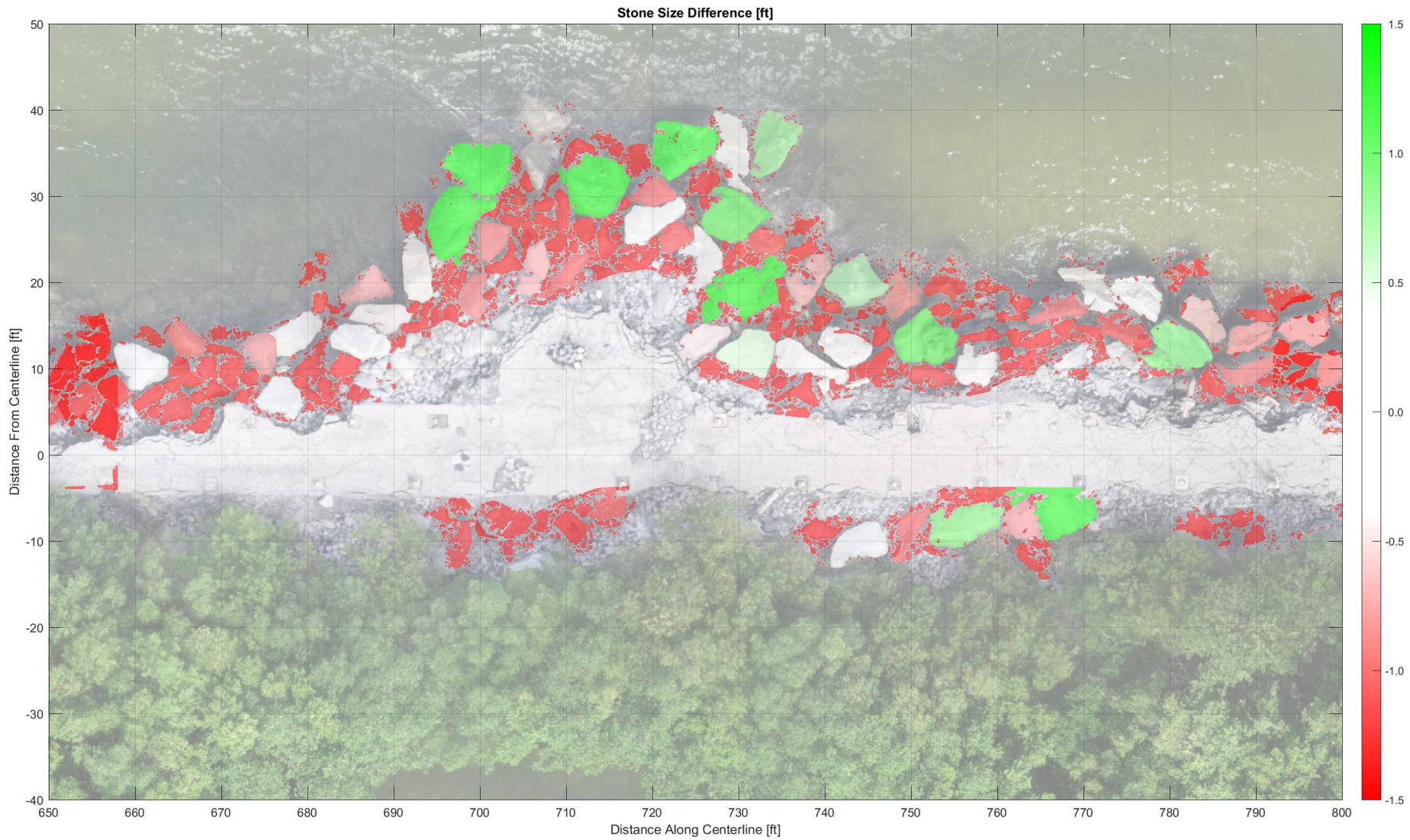


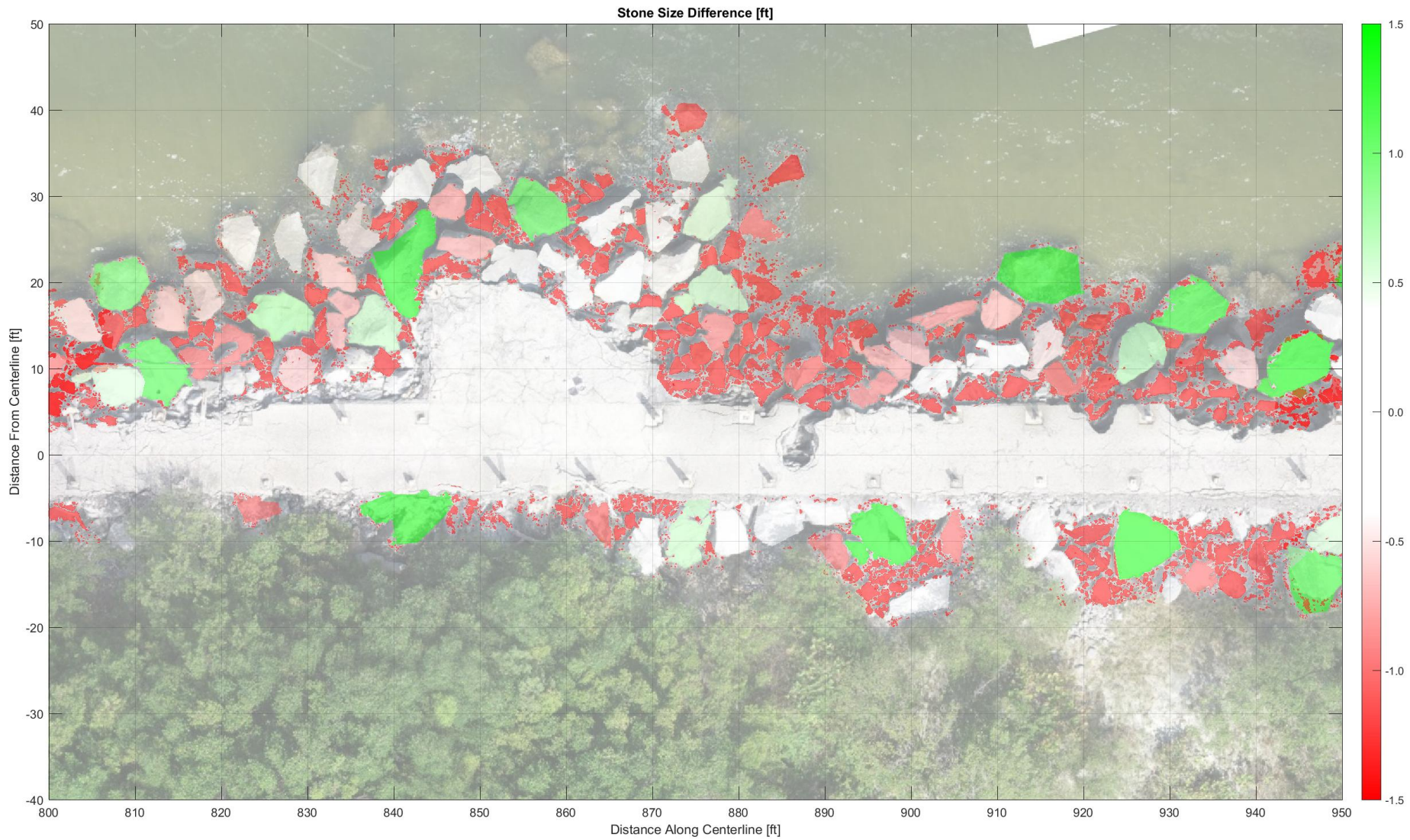


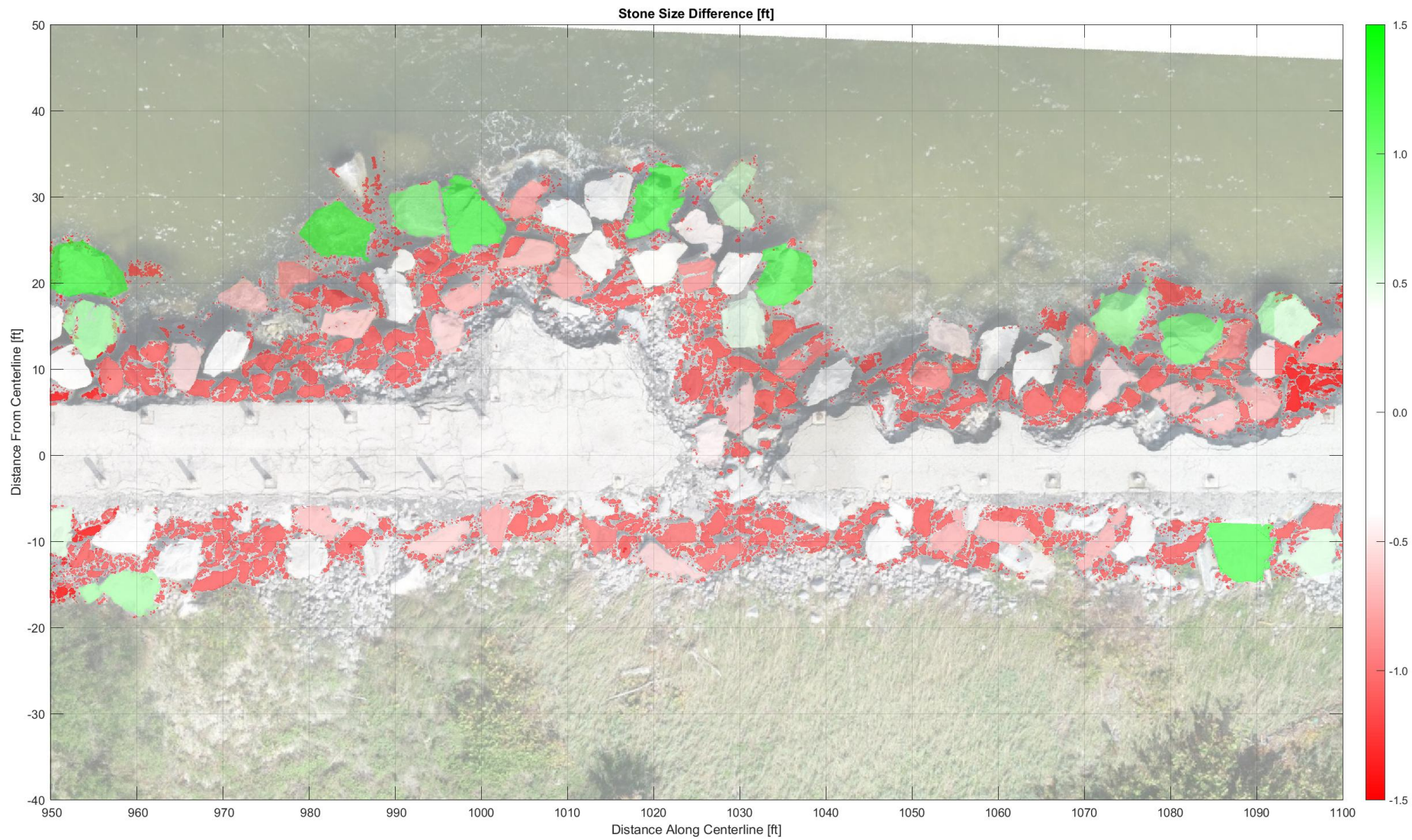


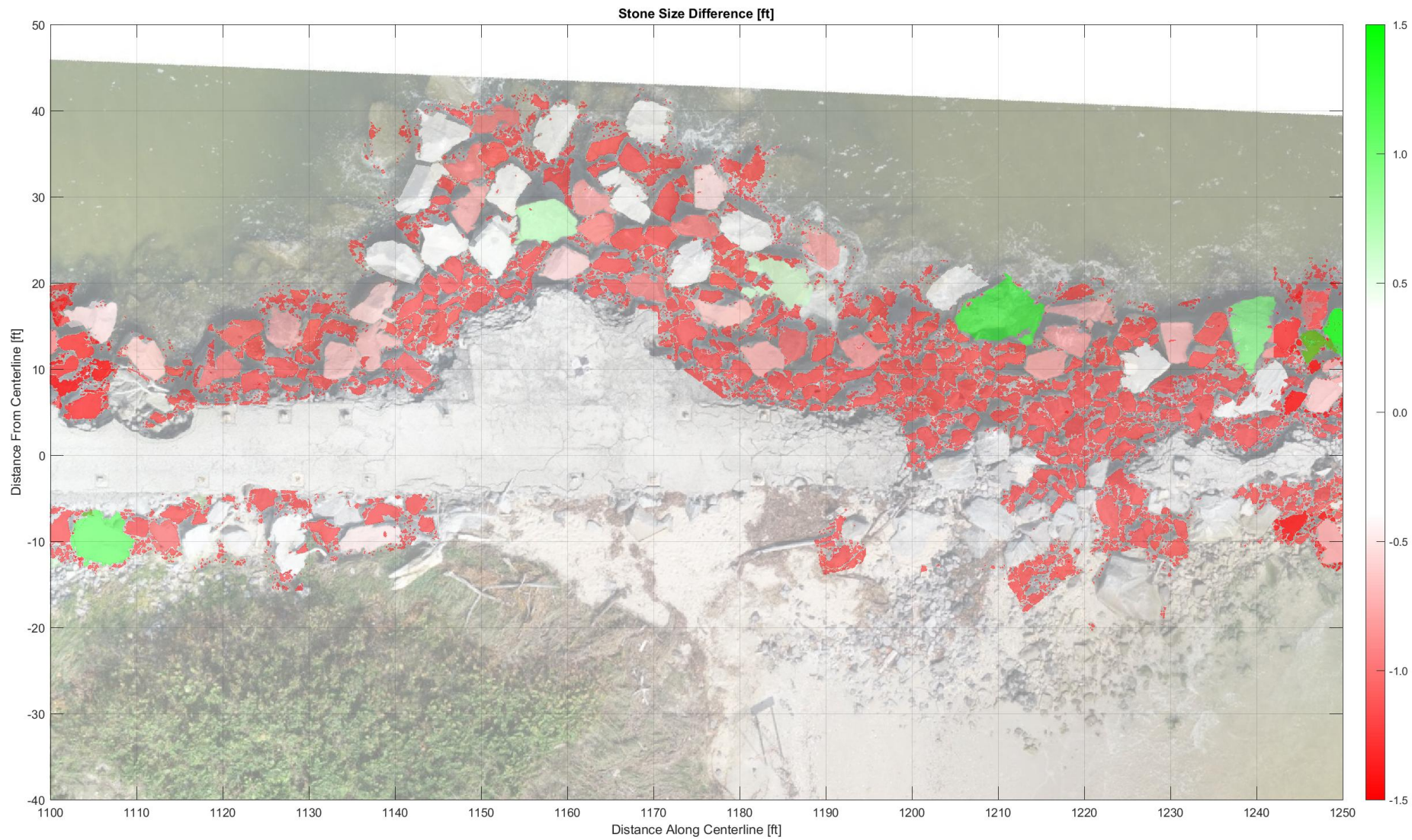


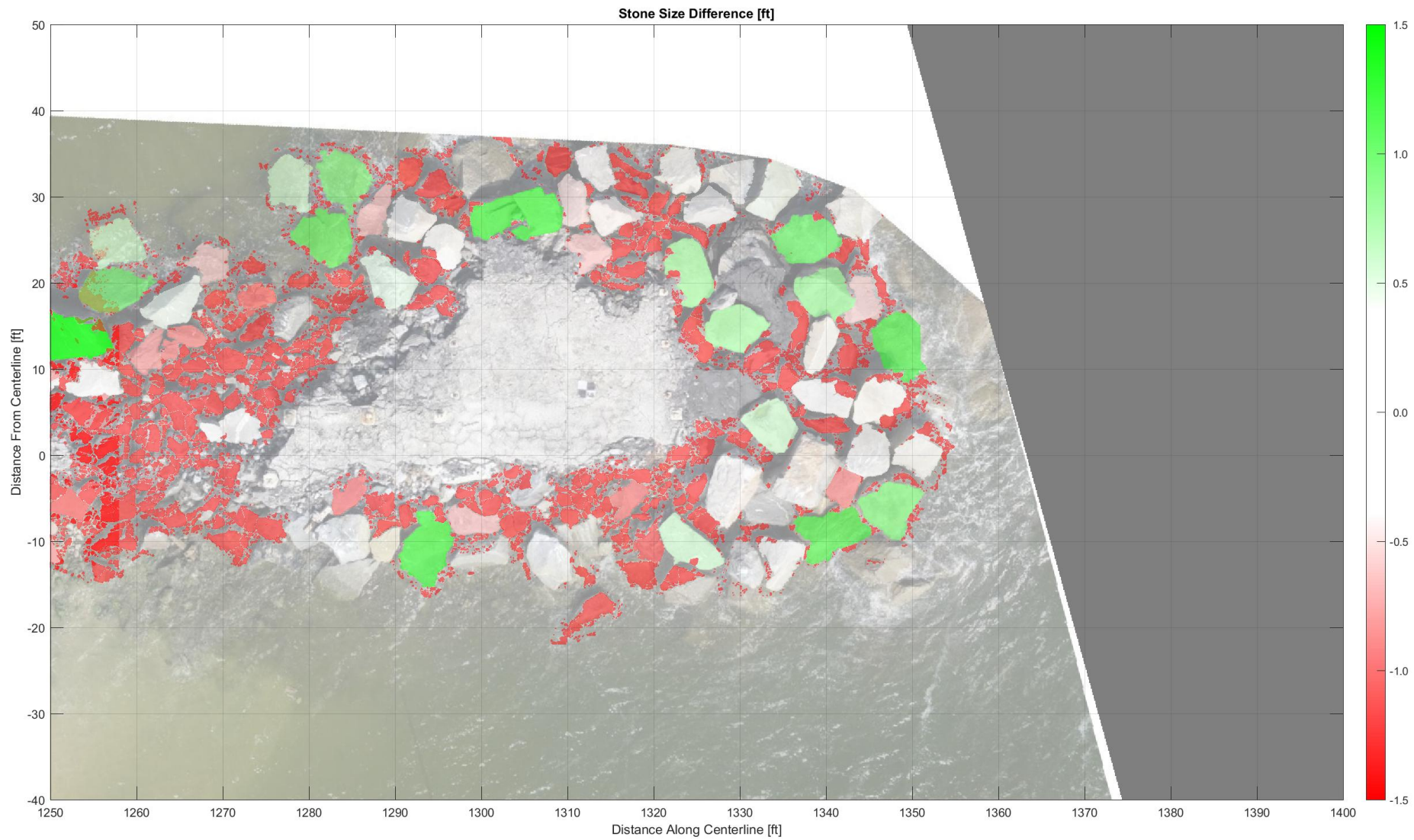






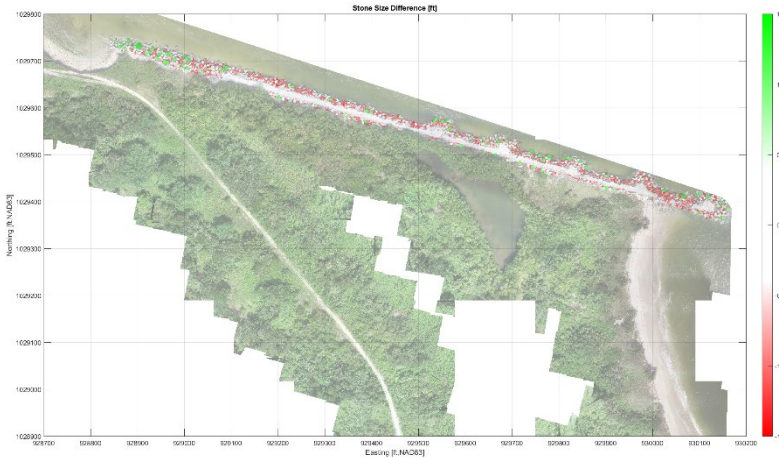








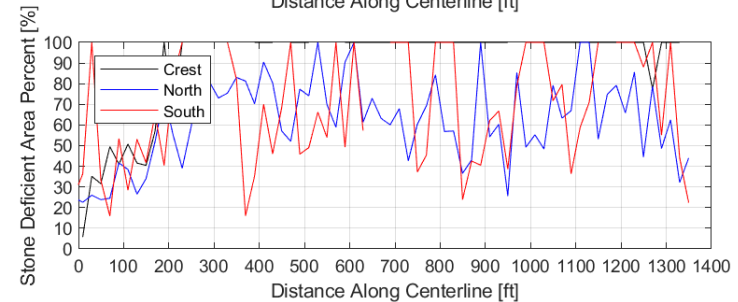
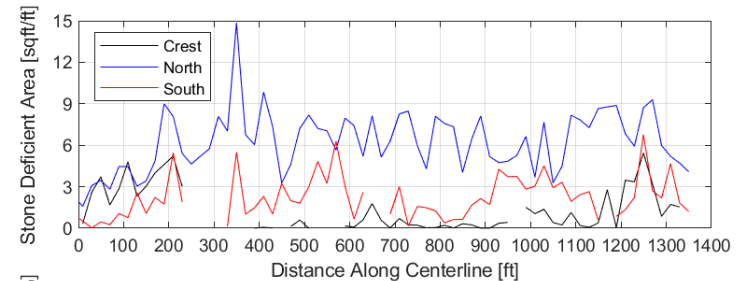
# JETTY STONE COMPARISONS



- › Armor stone size deficiencies were calculated for each 20-foot segment along the jetty crest and north and south jetty faces.

## › Stone Size Deficiency (sqft)

Face	Analyzed	Deficient	Percent
Crest	2,350	1,750	50%
North	14,350	8,850	62%
South	5,740	3,470	60%
<b>Total</b>	<b>22,440</b>	<b>8,950</b>	<b>60%</b>



# SUMMARY OF EXISTING CONDITIONS

## › Key Observations

- Large breach is present on seaward end
- 85% of jetty crest is below design elevation
- 60% of existing armor stone is undersized
- Maintenance road has deteriorated
- Side slopes have flattened

## › Conclusions

- Findings confirm that the structure has been damaged and is need of repair.
- Damage may be due to structural settlement, storm forces, or a combination of the two.



# CONCLUSIONS

- › Improves qualitative assessment while decreasing field time.
- › Potential use during construction for QA/QC.
- › Still need to visit site to evaluate armor interlocking.
- › Limited in mapping top-view conditions
  - Cannot be used to evaluate subsurface conditions



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# THANK YOU

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